

ENHANCED SHALLOW MARSH SYSTEM

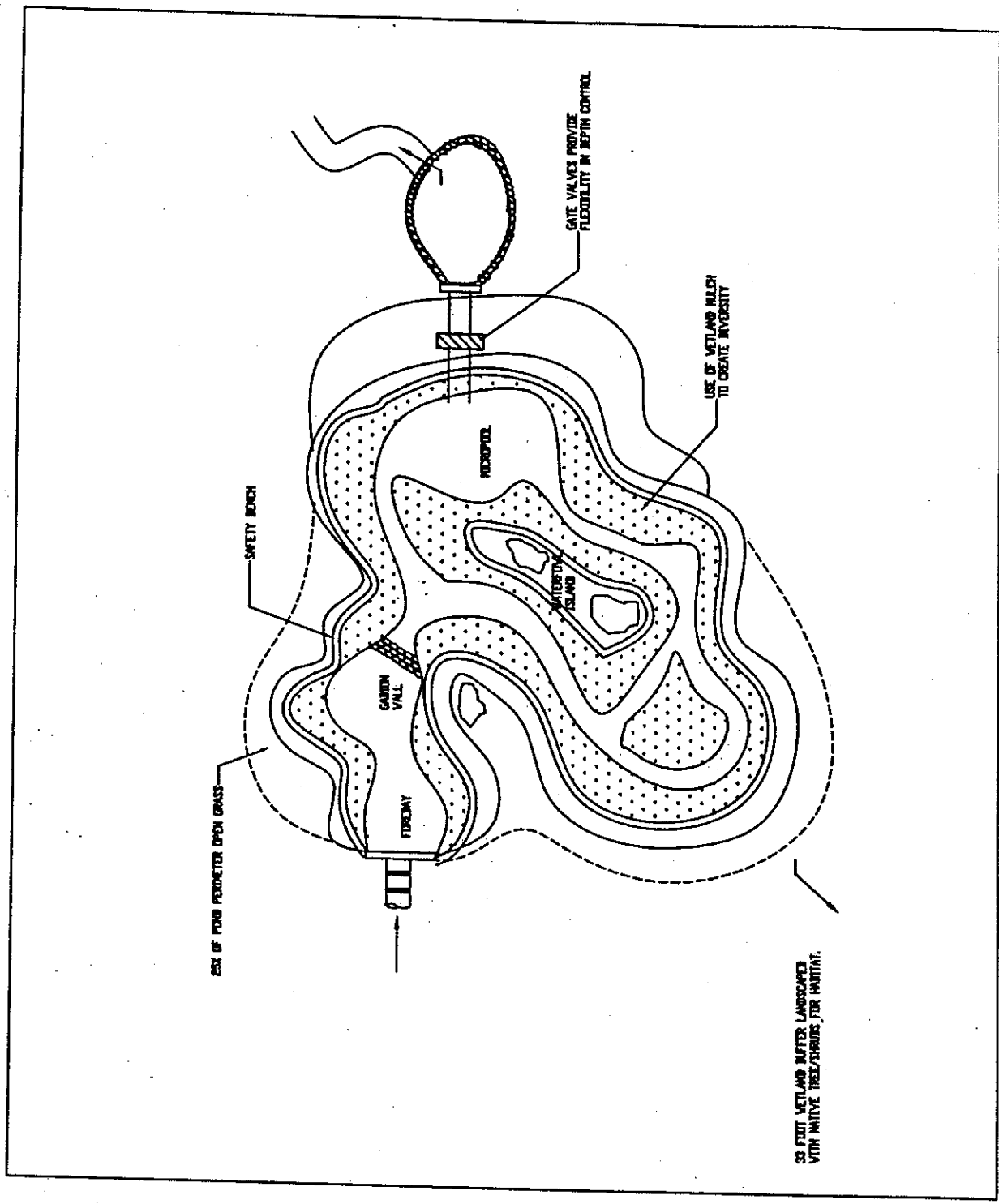
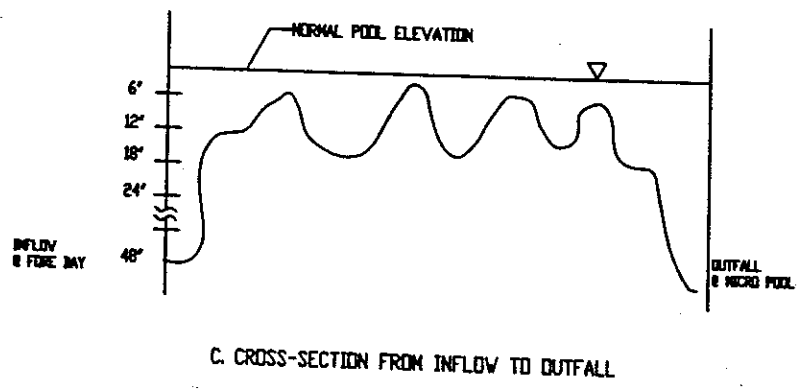
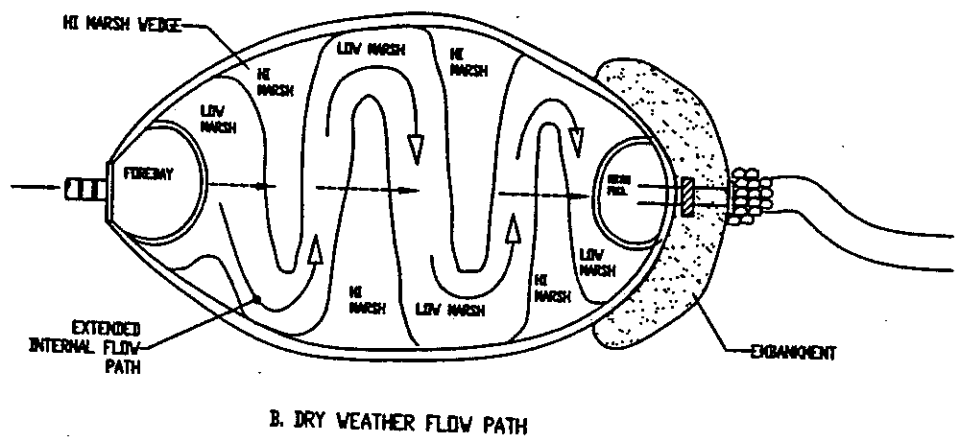
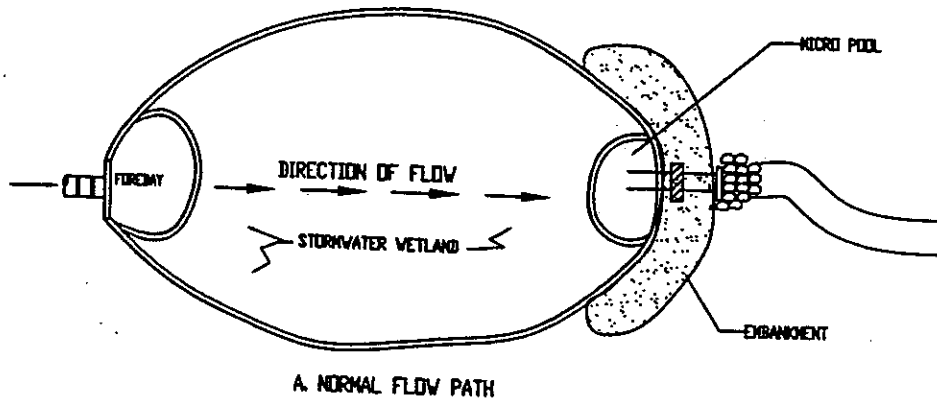


FIGURE 2-9-1

USE OF HI MARSH WEDGES TO EXTEND THE INTERNAL FLOW PATH THROUGH A STORMWATER WETLAND



Although the flow path of runoff during storms is governed by the distance between the inlet and outlet of the pond the effective flow path during dry weather can be much greater if wedges of H marsh (1 to 6 inches) are placed at right angles to the normal direction of flow.

FIGURE 2.9-2 USE OF PLACEMENT OF HIGH MARSH IN WETLAND SYSTEMS.

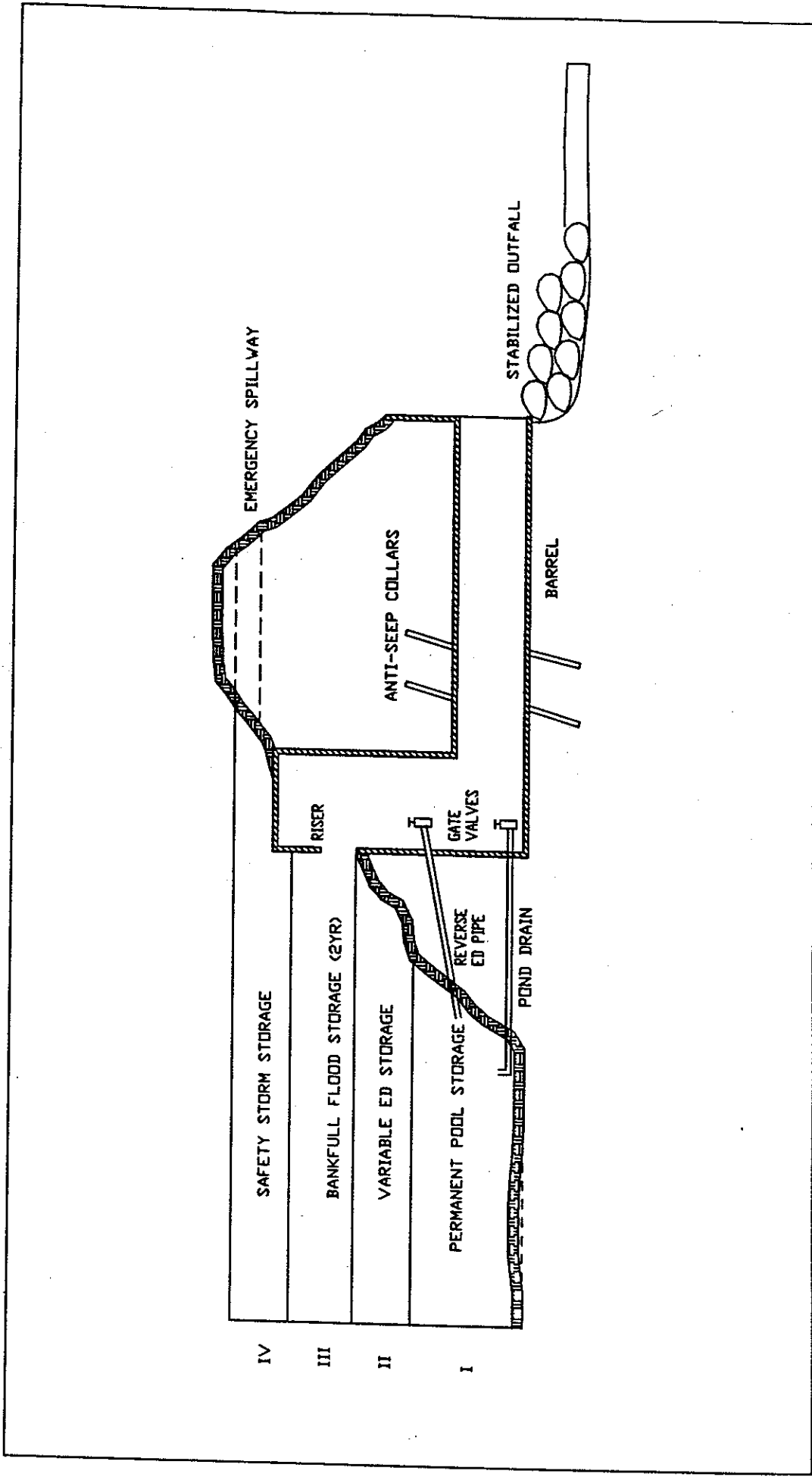
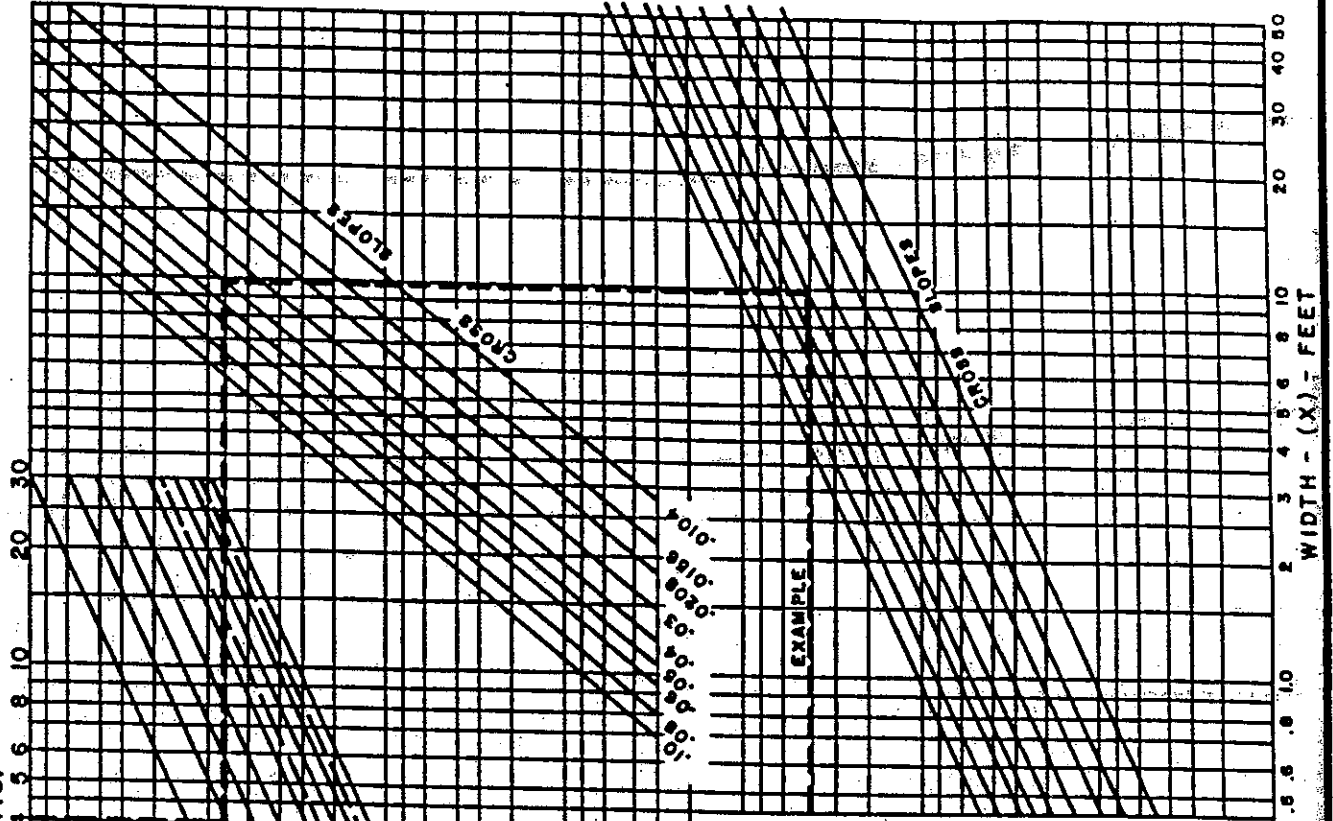


FIGURE 2.9-3 CROSS-SECTION VIEW OF A STANDARD ED POND SYSTEM DESIGN

DISCHARGE - (Q) - C.F.S.



DEPTH AT CURB - (Y) - FEET

INSTRUCTIONS

1. ENTER FIGURE AT TOP WITH DISCHARGE, Q
2. MOVE DOWN TO INTERSECT KNOWN LONGITUDINAL GUTTER GRADE (GUTTER SLOPE) LINE.
3. MOVE RIGHT TO INTERSECT KNOWN PAVEMENT CROSS SLOPE LINE.
4. MOVE DOWN TO INTERSECT PAVEMENT CROSS SLOPE LINE. (SAME VALUE AS IN 3 BUT A DIFFERENT LINE).
5. READ WIDTH OF FLOW AT BOTTOM AND DEPTH OF FLOW (Y) AT CURB AT LEFT.
6. PROCEDURE MAY BE REVERSED BY ENTERING WITH A KNOWN OR ASSUMED DEPTH (Y) OR WIDTH (Q).

TOWN OF SOUTH WINDSOR
 STANDARD DETAIL
 JANUARY, 1991

FLOW CHARACTERISTIC CURVES
 (STRAIGHT CROSS SLOPES WITH CURB)
 n = 0.015
 (CHART 1)

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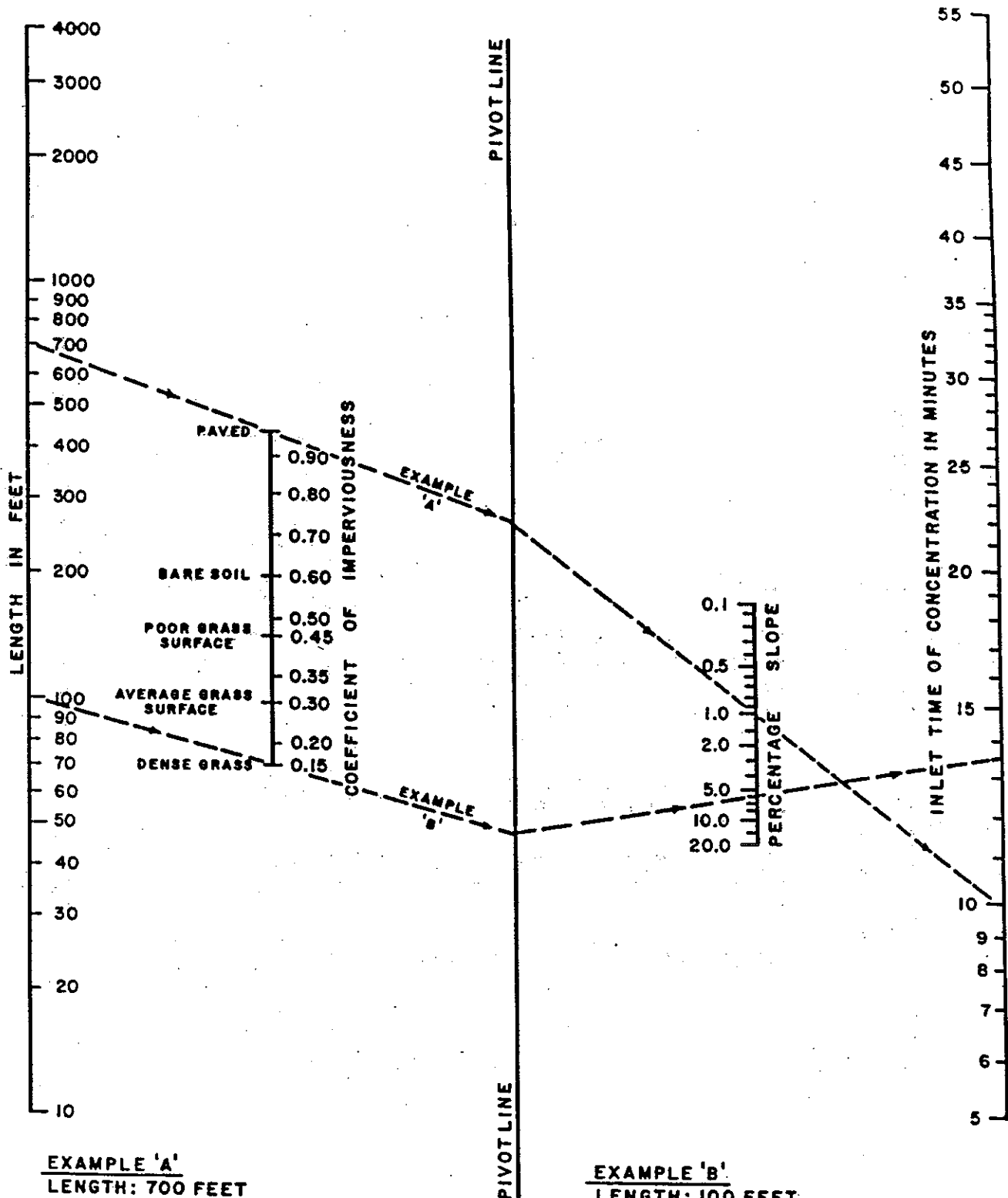
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RAINFALL INTENSITY CHART IN INCHES PER HOUR
HARTFORD, CT

STORM (YRS)	MINUTES																															
	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32				
2	4.1	3.8	3.6	3.4	3.2	3.1	3.0	2.9	2.8	2.6	2.5	2.4	2.3	2.3	2.2	2.2	2.1	2.1	2.0	2.0	1.9	1.9	1.8	1.8	1.7	1.7	1.7	1.7	1.7			
10	6.2	5.6	5.4	5.3	5.0	4.7	4.5	4.4	4.3	4.1	4.0	3.9	3.8	3.7	3.5	3.4	3.3	3.3	3.2	3.2	3.1	3.0	2.9	2.9	2.8	2.7	2.6	2.6	2.6			
25	7.1	6.7	6.4	6.1	5.7	5.6	5.4	5.2	5.0	4.9	4.7	4.5	4.4	4.3	4.2	4.1	4.0	4.0	3.9	3.8	3.7	3.6	3.5	3.5	3.4	3.3	3.2	3.2	3.2			
50	7.7	7.4	7.0	6.7	6.5	6.1	6.0	5.8	5.6	5.4	5.2	5.1	5.0	4.9	4.7	4.6	4.5	4.4	4.3	4.3	4.2	4.1	4.0	3.9	3.8	3.7	3.6	3.6	3.6			
100	8.4	8.0	7.6	7.3	7.0	6.8	6.6	6.4	6.2	6.0	5.8	5.6	5.4	5.2	5.1	5.0	4.9	4.8	4.7	4.6	4.5	4.4	4.3	4.2	4.1	4.0	3.9	3.8	3.8			

STORM (YRS)	MINUTES																															
	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60				
2	1.6	1.6	1.6	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1.1	1.1	1.1	1.1			
10	2.6	2.5	2.5	2.5	2.4	2.4	2.3	2.3	2.3	2.2	2.2	2.1	2.1	2.1	2.0	2.0	2.0	2.0	1.9	1.9	1.9	1.9	1.8	1.8	1.8	1.8	1.8	1.8	1.8			
25	3.1	3.1	3.0	3.0	2.9	2.9	2.8	2.8	2.7	2.6	2.5	2.5	2.5	2.5	2.4	2.4	2.4	2.4	2.3	2.3	2.2	2.2	2.2	2.2	2.2	2.1	2.1	2.1	2.1			
50	3.5	3.4	3.3	3.3	3.2	3.2	3.1	3.1	3.0	3.0	2.9	2.9	2.8	2.8	2.7	2.7	2.7	2.7	2.6	2.6	2.5	2.5	2.4	2.4	2.4	2.4	2.4	2.4	2.3			
100	3.8	3.7	3.7	3.6	3.6	3.6	3.5	3.5	3.4	3.4	3.3	3.3	3.2	3.2	3.2	3.1	3.1	3.0	2.9	2.9	2.8	2.8	2.7	2.7	2.7	2.7	2.6	2.6	2.6			

CHART 2



EXAMPLE 'A'
 LENGTH: 700 FEET
 PAVED
 SLOPE: 1.0 %
 TIME: 10 MINUTES

EXAMPLE 'B'
 LENGTH: 100 FEET
 DENSE GRASS
 SLOPE: 6.0 %
 TIME: 13 1/2 MINUTES

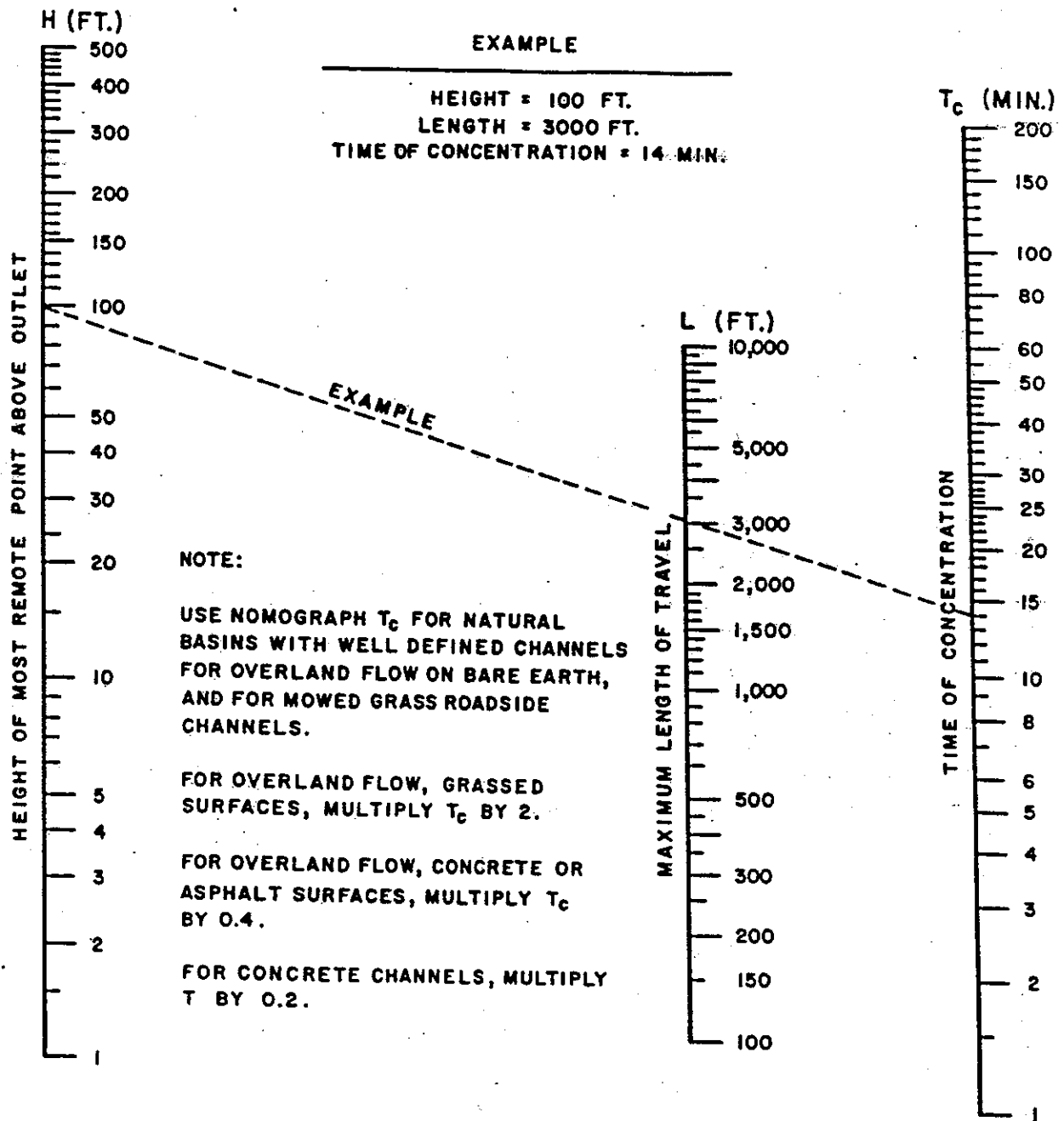
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 STANDARD DETAIL
 JANUARY, 1991

NOMOGRAPH FOR DETERMINING
 TIME OF CONCENTRATION
 (CHART 3)

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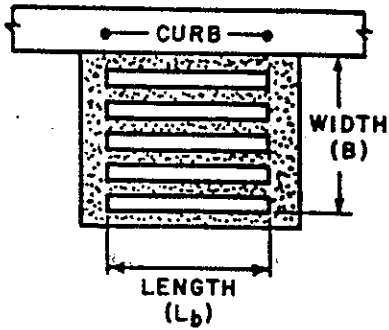
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KIRPICH CHART
TIME OF CONCENTRATION
(CHART 4)

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$$P = 2B + L_b$$

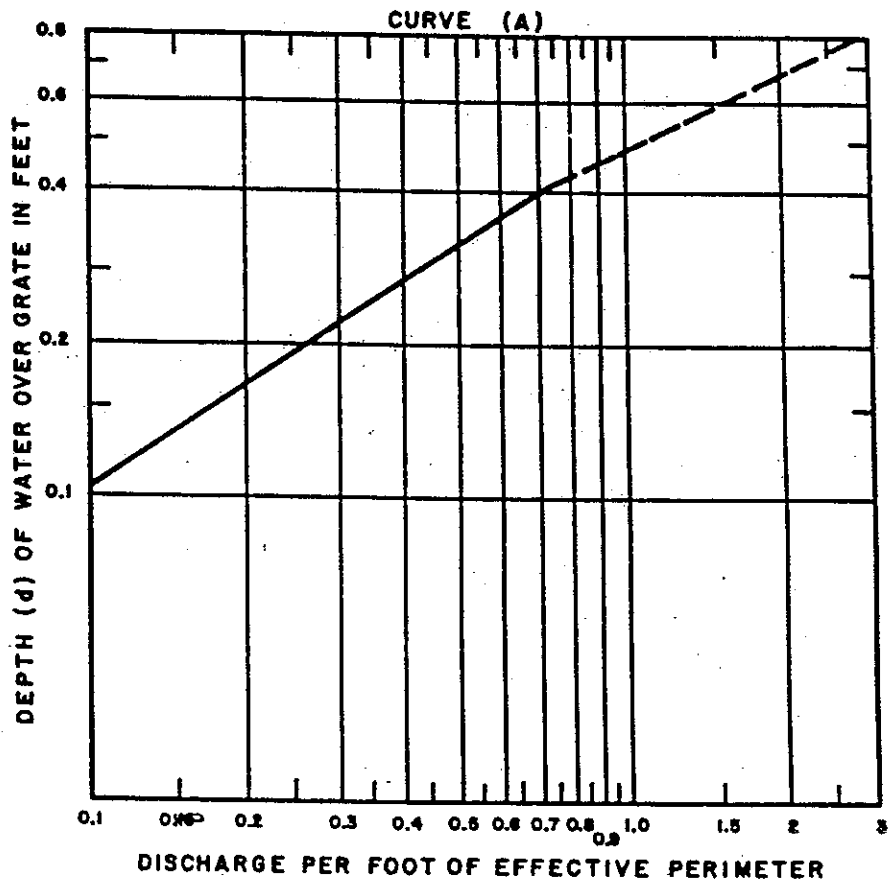
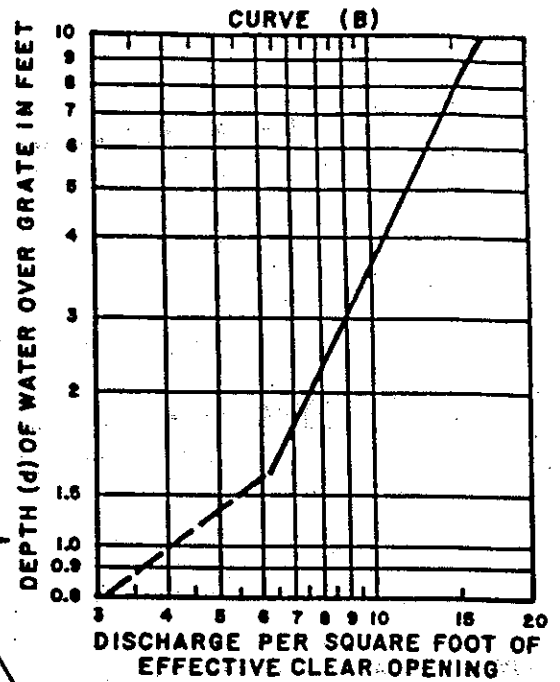
A = AREA OF CLEAR OPENING IN GRATE

TO ALLOW FOR CLOGGING, DIVIDE P OR A BY 2 BEFORE OBTAINING d.

WITHOUT CURB, $P = 2(B + L_b)$

USE CURVE (B) FOR DEPTHS OVER GRATE MORE THAN 0.8 FT.

USE CURVE (A) FOR DEPTHS OVER GRATE LESS THAN 0.8 FT.



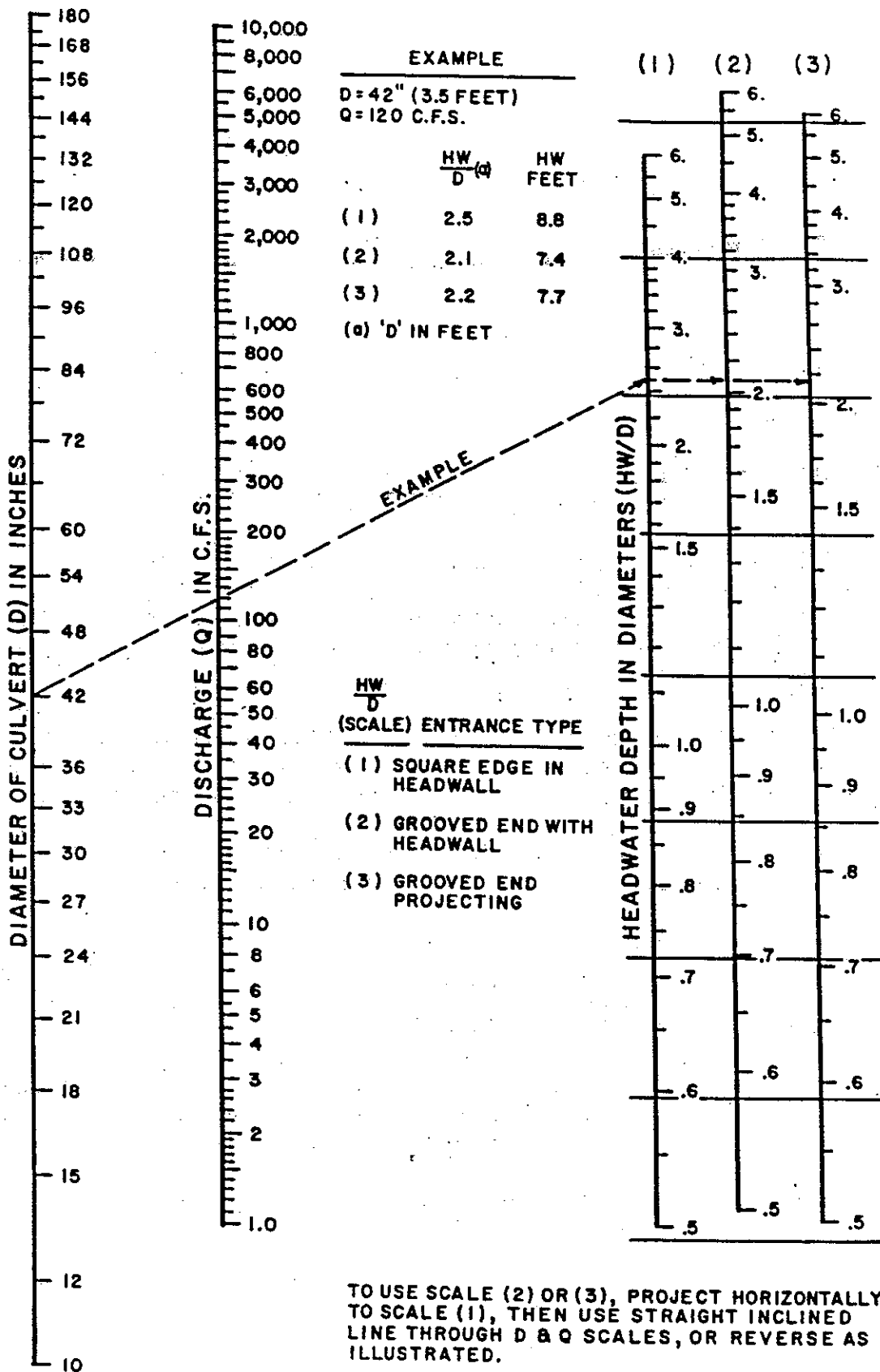
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JANUARY, 1991

HYDRAULIC CAPACITY OF
GRATE INLET IN SUMP
(CHART 5)

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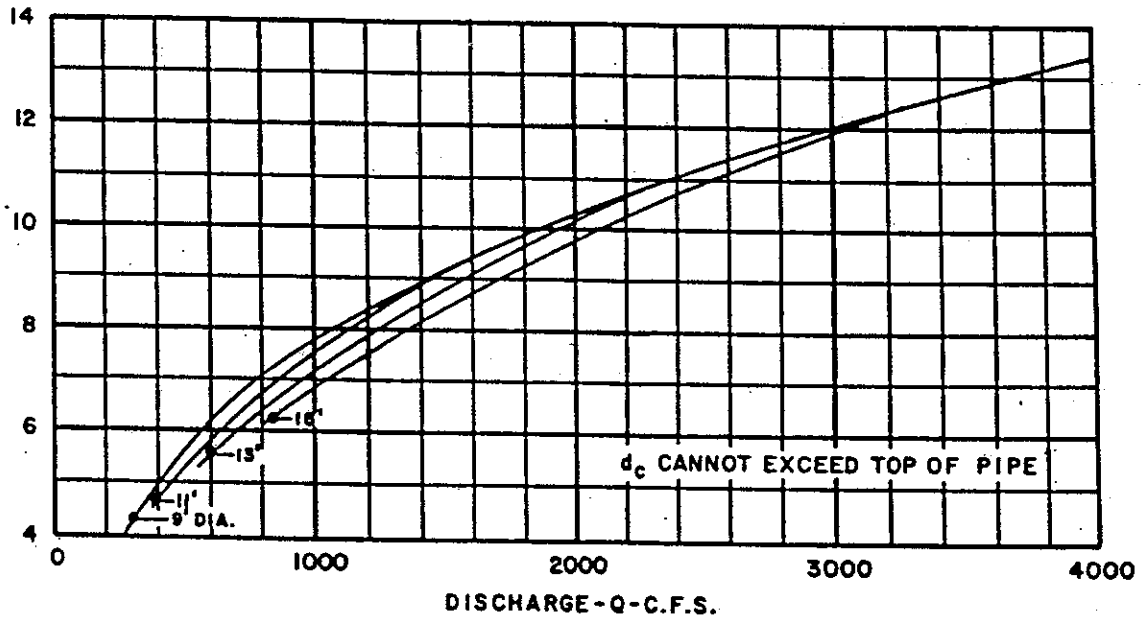
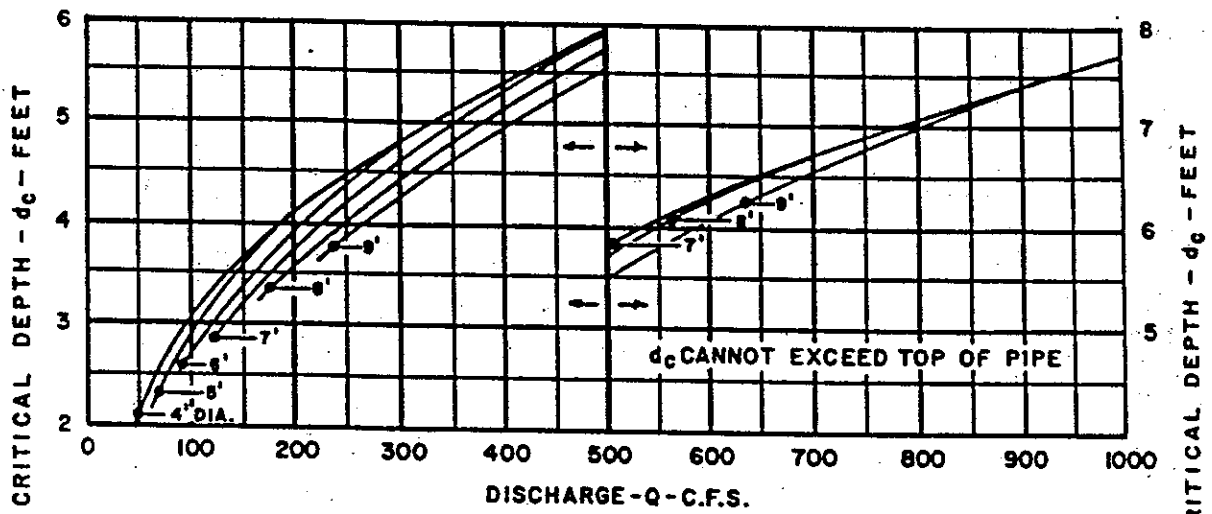
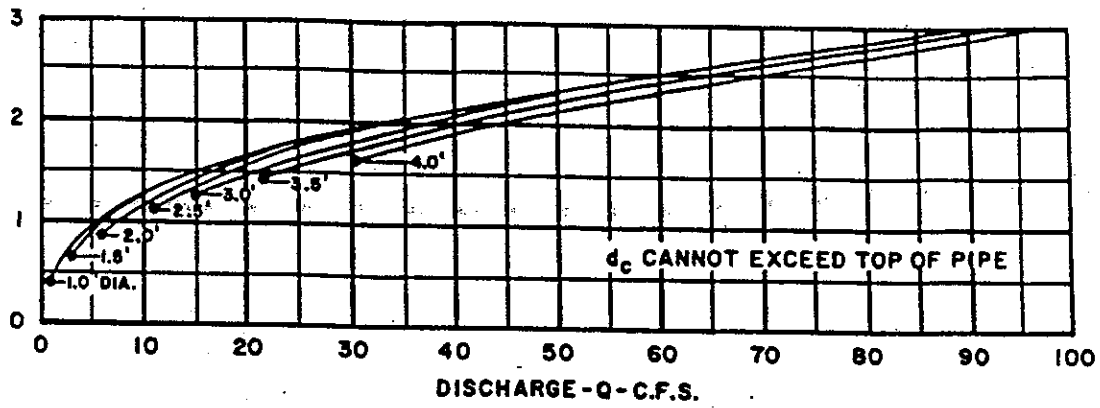
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TO USE SCALE (2) OR (3), PROJECT HORIZONTALLY TO SCALE (1), THEN USE STRAIGHT INCLINED LINE THROUGH D & Q SCALES, OR REVERSE AS ILLUSTRATED.

<p>TOWN OF SOUTH WINDSOR STANDARD DETAIL JANUARY, 1991</p>	<p>HEADWATER DEPTH FOR CONCRETE PIPE CULVERTS WITH INLET CONTROL (CHART 6)</p>	<p>APPROVED</p> <hr/> <p>PUBLIC WORKS DIRECTOR</p>
<p>REVISED:</p>		



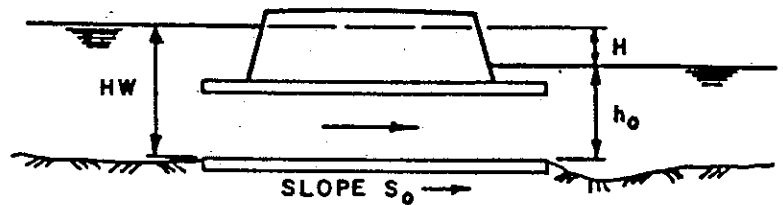
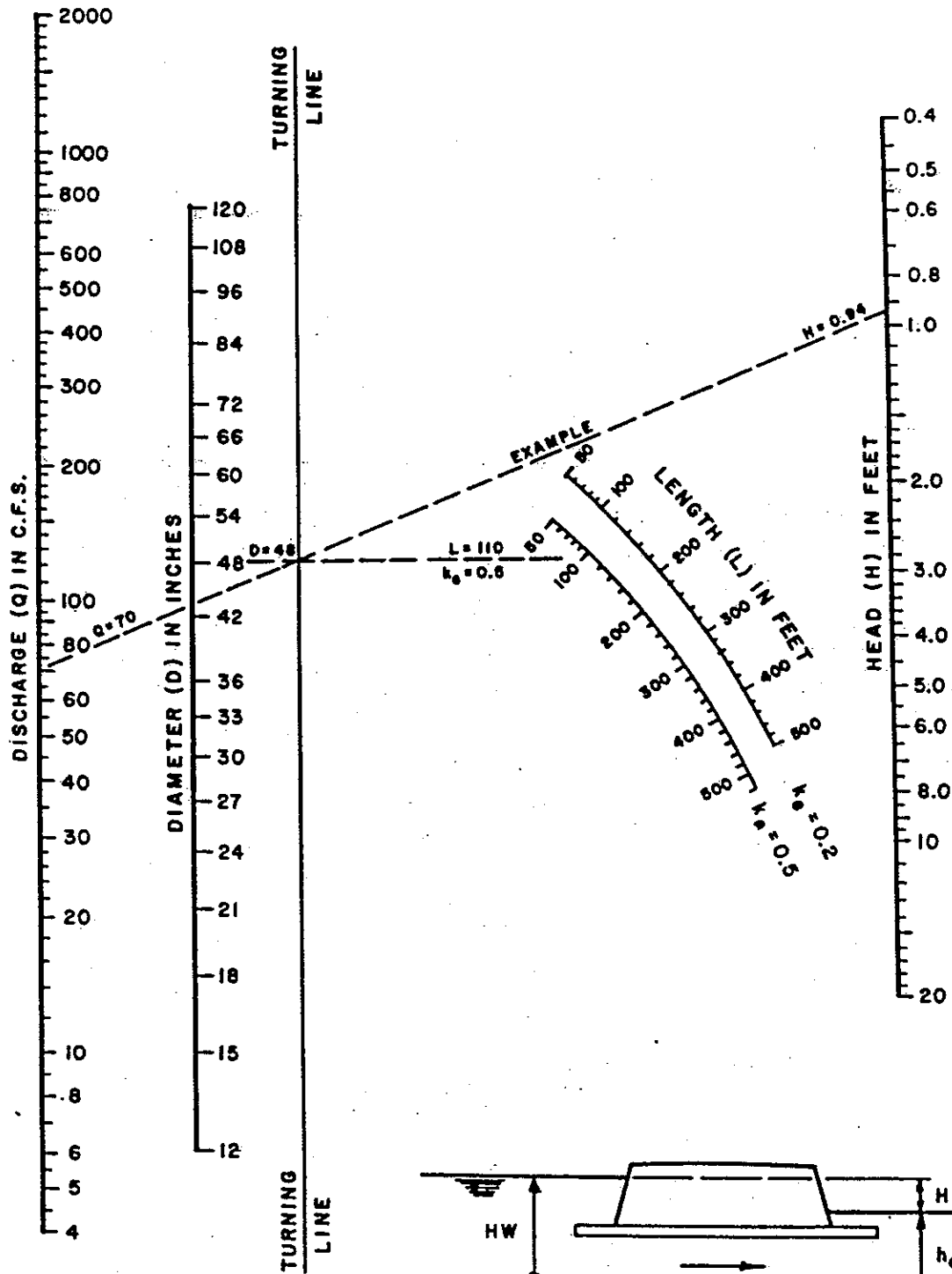
TOWN OF SOUTH WINDSOR
 STANDARD DETAIL
 JANUARY, 1991

CRITICAL DEPTH
 CIRCULAR PIPE
 (CHART 7)

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SUBMERGED OUTLET CULVERT FLOWING FULL

$$HW = H + h_0 - LS_0$$

For outlet crown not submerged, compute HW by methods described in the design procedure.

TOWN OF SOUTH WINDSOR
STANDARD DETAIL
JANUARY, 1991

HEAD FOR CONCRETE PIPE
CULVERTS FLOWING FULL
 $n = 0.012$ (CHART 8)

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