

### **Brooks Acoustics Corporation**

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Mr. Bradford H. Wainman UW Vintage Lane II, LLC P. O. Box 504 South Glastonbury, CT 06073 23 November 2021

Subject: Talbot Lane Development – Warehouse truck sound evaluation

Dear Mr. Wainman:

As requested, Brooks Acoustics Corporation (BAC) has conducted a sound evaluation study for the proposed Talbot Lane Development warehouse project in South Windsor, Connecticut.

As part of this study an evaluation will be made of the potential sound generated by a truck at the proposed Talbot Lane warehouse development in South Windsor, CT. This evaluation focused on the sound level at the nearest residential property line to the south. Those results were compared to provisions of the Town of South Windsor noise ordinance and the State of Connecticut noise regulations.

This study was based on project design information supplied on the project which are part of the Planning and Zoning application for the *Talbot Lane Development*.

Calculations of truck generated sound at the southernmost loading dock position were made for the nearest residential property line, at 124 Edgewood Drive. This analysis also included the beneficial effects of sound control design features which are included in the facility design. The calculations included a 12 foot sound barrier wall next to the loading dock area, and a 6 foot earthen berm and about 90 feet of vegetation and landscape plantings along the facility southern property line.

The maximum estimated sound level at the south residential property line from the truck activity is 43 dBA.

Significantly, this estimated sound level is *below* the regulatory limits for the Town of South Windsor and the State of Connecticut. Therefore, the truck is expected to be in compliance with regulatory requirements.

The study findings are summarized herein.

#### Estimates of sound level at the property line and neighbor residence

Acoustical calculations were made to estimate the sound level from truck activity at the proposed warehouse.

The **sound source** under consideration is a truck at the southernmost loading dock bay in the proposed Talbot Lane warehouse development. The source sound levels used for this analysis are based on sound test data provided by the US Federal Highway Administration (FHWA).

The sound level generated by a heavy truck in full throttle mode will depend on the speed of the truck. These sound levels are described in the US Federal Highway Administration, Traffic Noise Modeler (TNM) Technical Manual, as shown in the graph below for a distance of 50 feet, for various pavement types.

TNM is the sound modeler mandated to evaluate vehicle generated noise for all federal highway and many state highway projects.



The range of sound levels used by TNM goes from 80 dBA at under 10 MPH to about 90 dBA at 80 MPH. Note that CT State law (CGS 14-80a) prohibits noise emissions above 88 dBA at 50 feet for heavy trucks traveling at less than 35 MPH, so the TNM data are consistent with CT (and federal) law.

The TNM heavy truck sound spectrum shape at 10 MPH was used for this calculation, as shown below.



The truck activity was evaluated for potential impact on the neighborhood. The receiver location evaluated was the nearest residential property line to the south of the proposed development, at 124 Edgewood Drive.

A graphic showing the source to receiver conditions, including sound control features, is given below.

#### Truck in Existing & Loading bay Proposed **Buffer** Area nce from Dock - Truck Parking to Existing buffer of 50 ft mature **Residential Abutter Property Line = 274 ft** trees located along the southern property boundary with the residential abutter to LINLING remain and be augmented by under plantings Proposed additional buffer of foot perm planted both side 40 ft consisting of a 6 ft berm Natural (existing buffer) augmented with planted on both sides with Distance = 50 Feet evergreens under plantings Pi AA3 Residential 52 Abutter of NUCL Concern

The calculations included a 60 foot long and 12 foot high sound barrier wall next to the loading dock area, a 40 foot wide and 6 foot high earthen berm planted on both sides, and 50 feet of natural vegetation and landscape plantings along the facility southern property line.

The source sound and location data were used as input to a computer modeling procedure which calculated the propagation of that sound through the atmosphere to the receptor position. The sound propagation calculation procedure accounts for the effects of the sources, barriers, vegetation and also distance and atmospheric conditions, in accordance with International Standard on the attenuation of sound during propagation outdoors, ISO 9613-1.

The site plan of the facility is shown on the Site Plan Application for 25 Talbot Lane, drawing set Revision 6, dated November 17, 2021, prepared by Design Professionals, Inc. of South Windsor, CT.

The source sound data are shown on the calculation Source Sheet, attached. The path and receiver calculations sheets which indicate the calculation results are also attached. Conservatively estimated sound barrier effects for the facility and the barrier walls are shown in the attached Barrier Attenuation Calculation sheets for the sound barrier wall and for the earthen berm, respectively.

The receiver sheets show the contribution for the truck sound source, and also show the total received sound level at the receiver location.

The calculation results are summarized below:

Sound Source	Distance	Sound level
Truck in southernmost loading bay	50 feet	80 dBA
Maximum Truck Sound Level (With Sound Control Features)	Distance	Sound level
124 Edgewood Drive property line	274 feet	43 dBA

Significantly, the estimated truck sound level at the north property line of 43 dBA is in compliance with both the Town of South Windsor Noise Ordinance (Article III, Section 50-65 Performance standards) and the Regulations of Connecticut State Agencies (RCSA 22a-69 Control of Noise). For both the Town of South Windsor and the State of CT the sound level limit for industrial sources at a residential receiver property line is 61 dBA during daytime hours (7 am to 10 pm) and 51 dBA during nighttime hours (10 pm to 7 am).

The study shows that the truck sound will meet the required limit of 51 dBA during the nighttime hours (10 pm to 7 am). So, the truck sound is expected to be *in compliance* with all regulatory requirements.

#### **Discussion**

The proposed sound mitigation features are expected to provide significant reductions in sound levels from the truck loading dock to the south residential property line. It is important to note that the truck sound level will *drop substantially* for houses at greater distances.

Please contact me if you have any questions concerning these findings.

Very truly yours, BROOKS ACOUSTICS CORPORATION

Bennett M. Brooks, PE, FASA, INCE President

Attachments



## **APPENDIX**

1- **Sound Projection Data** Sound source sheet Sound path and receiver sheets Barrier calculations

Source Group: Source Name: Source Data: Source Level: record distance: Source Type:	E She Facility Truck at docl US FWHA 75 dB(A) 50	et A-wt	Fley	Facility 80 70 60 60 50 40 30 20 10 0 51 20 10 0 51 20 10 10 50 20 10 50 20 50 20 50 20 50 20 50 20 50 20 50 20 50 20 50 20 50 20 20 20 20 20 20 20 20 20 20 20 20 20	r : Truck at dock
Coordinates:	0	0	8		Octave Band Center Freq. (HZ)
		Atten		A-weighted	A-weighting
Frequency	Data	Berm	Signature	Signature	Curve freq.
31.5 Hz 63.0 Hz 125.0 Hz 250.0 Hz 500.0 Hz 1000.0 Hz 2000.0 Hz	32.5 59.9 68.6 71.8 74.5 75.5 73.6 70.6	5 5 5 5 5 5 5	28 55 64 67 70 71 69 66	-12 29 48 58 66 71 70 67	$\begin{array}{cccc} -39.4 & 31.5 \\ -26.2 & 63 \\ -16.1 & 125 \\ -8.6 & 250 \\ -3.2 & 500 \\ 0.0 & 1000 \\ 1.2 & 2000 \\ 1.0 & 4000 \end{array}$

US FWHA TNM Data

Truck @ 10 MPH max SPL 80 dBA @ 50 ft

> 6 ft earth berm BAC calc Atten ~5 dBA

#### BAC Project Letter PJ2021-1376-L01

#### **Talbot Lane Development**

#### Property Line Sound Study

#### Sound Projection: Truck at loading dock

PROJECTED FROM: Loading dock

Based on FWHA sound data and proposed site plan

South Residential Property Line

Facility layout with sound control

		Coordinates:		
OJECTED FROM: Loading dock	East	North	Elevation	
PROJECTED TO: South residential property line	137.0	-237.3	5.0	

RELATIV TEN ATN	E HUMIDITY: 509 IPERATURE: 72 IOS. PRESS: 760	% deg. F ) mm Hg	Criteria Level 45 dBA Total Sound Level 43 dBA	Compliance? YES
				CONTRIBUTIONS
FREQ.	<u>AWT SPL</u>		SOURCE	AWT SPL
31.5 Hz	-36.5	#		
63 Hz	3.1	1	Facility Truck at do	ck 42.6 dBA
125 Hz	25.3	2	reserved	-42.5 dBA
250 Hz	35.5	3	reserved	-42.5 dBA
500 Hz	39.1	4	reserved	-42.5 dBA
1000 Hz	36.5	5	reserved	-42.5 dBA
2000 Hz	31.8	6	reserved	-42.5 dBA
4000 Hz	25.0	7	reserved	-42.5 dBA
8000 Hz	7.5	8	reserved	-42.5 dBA
		9	reserved	-42.5 dBA
RMS:	42.6	10	reserved	-42.5 dBA
		11	reserved	-42.5 dBA
		12	reserved	-42.5 dBA

Atmospheric attenuation:	yes
Excess gound attenuation:	yes
Source region hard, soft, mixed (h,s,m%):	h
Receiver region hard, soft, mixed (h,s,m%):	s
Middle region hard, soft, mixed (h,s,m%):	s
Barrier shadowing:	yes
Vegetation	yes

#### PATH SHEET

			<u>CO</u>	ORDINATES					
SOURCE 1: F	acility		East	0.0			Record Distance		
Т	ruck at dock		North	0.0			50.0		
TYPE: p	oint		Elevation	8.0			Projection Dist.		
							274.0		
					Net				
Freq.	Source	Vegetation	Shadowing	Ground Atten	Barrier Atten	Atmospheric	Distance Atten	Contribution	Awt Contrib.
31.5 Hz	27.7	0.7	6.2	-3.0	9.2	0.0	14.8	2.9	-36.5
63 Hz	55.1	0.7	7.2	-3.0	10.2	0.0	14.8	29.3	3.1
125 Hz	63.8	1.1	8.8	2.3	6.5	0.0	14.8	41.4	25.3
250 Hz	67.0	1.5	10.8	4.2	6.6	0.1	14.8	44.1	35.5
500 Hz	69.7	1.5	13.3	2.4	10.9	0.2	14.8	42.3	39.1
1000 Hz	70.6	1.8	16.0	-1.0	17.0	0.4	14.8	36.5	36.5
2000 Hz	68.6	2.2	18.8	-1.5	20.3	0.8	14.8	30.6	31.8
4000 Hz	65.5	2.9	20.0	-1.5	21.5	2.3	14.8	24.0	25.0
8000 Hz	57.3	4.4	20.0	-1.5	21.5	8.0	14.8	8.6	7.5
								48.0	42.6

#### PATH SHEET

			<u>CO</u>	ORDINATES					
SOURCE 2: re	URCE 2: reserved East 0.0				Record Distance				
	-		North	0.0			1.0		
TYPE: po	oint		Elevation	1.0			Projection Dist.		
							274.0		
					Net				
Freq.	Source	Vegetation	Shadowing	Ground Atten	Barrier Atten	Atmospheric	Distance Atten	Contribution	Awt Contrib.
31.5 Hz	0.0	0.0	0.0	-2.0	-2.0	0.0	48.8	-46.8	-86.2
63 Hz	0.0	0.0	0.0	-2.0	-2.0	0.0	48.8	-46.8	-73.0
125 Hz	0.0	0.0	0.0	2.3	2.3	0.0	48.8	-51.1	-67.2
250 Hz	0.0	0.0	0.0	4.2	4.2	0.1	48.8	-53.0	-61.6
500 Hz	0.0	0.0	0.0	2.4	2.4	0.2	48.8	-51.4	-54.6
1000 Hz	0.0	0.0	0.0	-1.0	-1.0	0.4	48.8	-48.2	-48.2
2000 Hz	0.0	0.0	0.0	-1.5	-1.5	0.8	48.8	-48.1	-46.9
4000 Hz	0.0	0.0	0.0	-1.5	-1.5	2.3	48.8	-49.6	-48.6
8000 Hz	0.0	0.0	0.0	-1.5	-1.5	8.0	48.8	-55.3	-56.4
								-39.7	-42.5





#### BARRIER ATTENUATION CALCULATION Talbot Lane Development Source: Truck -- Receiver: Planted berm -- Barrier: 12 foot sound barrier wall

(\* Indicates values to be input in feet -- baseline elev. 76 ft)

h <sub>b</sub> := 12 h <sub>s</sub> := 8	*Height of barrier *Height of source	$d_{sb} := 3$ $d_{br} := 160$	*Distance from source to barrier *Distance from barrier to receiver
$h_r := 6$ $c_r := 344$	*Height of Receiver Speed of sound (m/s)	n := 0	) 8
$f_n \coloneqq 31.25 \cdot 2^n$	Frequency of peak (H;	z)	
$\lambda_n := \frac{c}{f_n}$	Wavelength of peak (r	neters)	
$D_{br} \coloneqq d_{br} \cdot .3048$	$D_{br} = 48.768$		
$D_{sb} := d_{sb} \cdot .3048$	$D_{sb} = 0.914$		
$\mathrm{H}_{sb} := \left(h_b - h_s\right)$	$H_{sb} = 1.219$		
$H_{br} := \left(h_b - h_r\right)$	$H_{br} = 1.829$	The path di geometry c	stances specific to the f the installation in meters
$\mathbf{R}_{sb} := \sqrt{\left(\mathbf{D}_{sb}\right)^2}$	$\overline{R_{sb}}^2 + (H_{sb})^2$ $R_{sb} = 1$	.524	
$R_{br} := \sqrt{D_{br}^2} +$	$-H_{br}^2$ $R_{br} = 4$	8.802	
$N_{n} := \frac{2 \cdot \left[ \left( R_{sb} \right) \right]}{2 \cdot \left[ \left( R_{sb} \right) \right]}$	$\frac{(1+R_{br}) - (D_{sb} + D_{br})}{\lambda_n}$	Fresnel Nu	mber
<u>C</u> := 10		C=10 for re (close to gr	eceiver over reflecting plane round)
A <sub>barrier</sub> := 10∙	$\log\left[3 + C \cdot N_n \cdot \exp\left[-\frac{1}{2000} \cdot \sqrt{\frac{1}{2}}\right]\right]$	$\frac{R_{sb} \cdot R_{br} \cdot \left(D_{sb} + D_{b}\right)}{\left[\left(R_{sb} + R_{br}\right) - \left(D_{sb} + R_{br}\right)\right]}$	$\overline{\left( \begin{array}{c} r \\ - \end{array} \right)}$ Barrier Attenuation
$A_{\text{barrier}} = \begin{pmatrix} 6.2\\ 7.2\\ 8.8\\ 10.3\\ 13.3\\ 16\\ 18.3\\ 21.3\\ 24.3 \end{pmatrix}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Note: Practical limit	for barrier attenuation is 20 dB



#### BARRIER ATTENUATION CALCULATION Talbot Lane Development

# Source: Planted Berm -- Receiver: South residential property line -- Barrier: Planted Berm (\* Indicates values to be input in feet -- baseline elev. 76 ft)

$h_b := 6$ $h_s := 6$ $h_r := 5$	*Height of barrier *Height of source *Height of Receiver		$d_{sb} := 1$ $d_{br} := 115$	*Distance from source to barrier *Distance from barrier to receiver
<u>c</u> .:= 344	Speed of s	sound (m/s)	n := 0	8
$f_n := 31.25 \cdot 2^{\frac{1}{2}}$	Frequency Wavelend	v of peak (Hz)	c)	
$r_n = f_n$	via volorigi		5)	
$D_{br} := d_{br} \cdot .304$	8 $D_{br} =$	= 35.052		
$D_{sb} := d_{sb} \cdot .304$	8 D <sub>sb</sub> =	= 0.305		
$H_{sb} := (h_b - h_s)$	)·.3048 H <sub>sb</sub> =	= 0		
$H_{br} := \left(h_b - h_r\right)$	)·.3048 H <sub>br</sub> =	= 0.305	The path dia geometry o	stances specific to the f the installation in meters
$R_{sb} := \sqrt{\left(D_{sb}\right)}$	$\left( H_{sb} \right)^2 + \left( H_{sb} \right)^2$	$R_{sb} = 0.305$		
$R_{br} := \sqrt{D_{br}^2}$	$+ H_{br}^{2}$	$R_{br} = 35.053$	;	
$N_n := \frac{2 \cdot \left[ \left( R_s \right)^{-1} \right]}{2 \cdot \left[ \left( R_s \right)^{-1} \right]}$	$\frac{1}{b_{b}+R_{br}}-\left(D_{sb}+D_{br}-\lambda_{n}\right)$	br)]	Fresnel Nu	nber
<u>C</u> := 10			C=10 for re (close to gr	ceiver over reflecting plane ound)
$A_{barrier_n} := 10$	$\log \left[ 3 + C \cdot N_n \cdot exp \right]$	$-\frac{1}{2000} \cdot \sqrt{\frac{R_s}{2 \cdot \left[ \left( R_{sb} \right)^2 + \frac{1}{2} \cdot \left[ \left( R_{sb} \right)^2 + \frac{1}{2} + \frac{1}{2}$	$\frac{\mathbf{b} \cdot \mathbf{R}_{br} \cdot \left(\mathbf{D}_{sb} + \mathbf{D}_{br}\right)}{\mathbf{b} + \mathbf{R}_{br} - \left(\mathbf{D}_{sb} + \mathbf{B}_{br}\right)}$	$\overline{D_{br}}$ Barrier Attenuation
$A_{barrier} = \begin{pmatrix} 4.3 \\ 4.4 \\ 4.4 \\ 4.4 \\ 4.5 \\ 5.5 \\ 5.7 \\ 5.4 \end{pmatrix}$	3 3 3 3 3 3 3 3 3 3 3 3 3 3	5 5 0 0 00 00 00 00	e: Practical limit	for barrier attenuation is 20 dB

