# Stormwater Management Report Hartford Truck Equipment 45, 95 John Fitch Boulevard & 542 King Street South Windsor, Connecticut

Prepared by:

Design Professionals, Inc. 21 Jeffrey Drive South Windsor, CT 06074

June 13, 2022



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#### **Introduction**

Hartford Truck Equipment, Inc. (current site occupant and affiliate of property owner McGuire Road Associates, LLC) is proposing site improvements to a tract of land comprised of three properties located at 45 & 95 John Fitch Boulevard, & 542 King Street, South Windsor, Connecticut. The properties are referenced on the Town of South Windsor Tax Assessors map as GIS#:47700045, 47700095, & 50400542 respectively. The proposed site improvements will include the construction of a new 45,000± SF storage building and a 10,000± building addition to their existing facility. Associated site improvements will include but not be limited to: new access driveways, parking areas for vehicles, sidewalks, landscaping, lighting, utilities, and stormwater management BMP's.

The total combined tract area is 15.54 acres. 8.20± acres of this area are proposed to be disturbed during construction. For more information, please refer to the plans entitled "Hartford Truck Equipment ~ Site Plan Modification ~ 45, 95 John Fitch Boulevard & 542 King Street ~ South Windsor, CT ~ GIS#: 50400542, 47700095, & 47700045" prepared by Design Professionals, Inc., and dated June 13, 2021, as amended.

#### **Pre-Development Site Conditions**

Apart from the existing develop area to be modified for the building addition, the existing surficial characteristics of the area to be improved can be primarily classified as undisturbed meadow area with some grass and woodland areas around the site boundary. Review of offsite topology indicated that the site currently accepts runoff from some of its southerly property abutters today. A ridgeline spanning south-west to north-east across the site's midsection was also identified as the main drainage divide on the property. Offsite runoff from the property's southerly abutters and the portion of the site east of the drainage divide, drain to an existing catch basin onsite. Collected stormwater it is then conveyed to an existing Catch Basin in King Street via a 42" RCP culvert. The portion of the site to the west of the drainage divide flows overland to this same catch basin.

The catchbasin in King Street was selected as the design point for our drainage analysis. This catch basin ultimately drains to The Podunk River and is a part of local basin ID 4004-00-2-R1. Existing conditions watershed delineations are identified in the Existing Conditions Drainage Map located in **Appendix G**. Based on Natural Resources Conservation Service (NRCS) Hydrologic Soil Group (HSG) mapping, soil types A, B, C, & D are located on site. See **Appendix C** for The NRCS Soil Map & Data.

An evaluation was performed to quantify the peak rate of stormwater discharge offsite to the design points identified. The Natural Resources Conservation Service's TR-55 Manual was followed in predicting the peak rates of runoff and volumes. HydroCAD computer modeling software was utilized.

Peak rates of stormwater runoff were evaluated for the 2-, 10-, 25-, 50- and 100-year storm events. Peak rates of stormwater runoff were evaluated for the 2-, 10-, 25-, 50- and 100-year storm events. Rainfall data from NOAA Atlas 14 Point Frequency Estimates was used to generate storm conditions. NOAA Atlas 14 rainfall data is included in **Appendix D** for reference. For more information, please refer to the enclosed Pre-Development Drainage HydroCAD Report located in **Appendix A**.

#### **Post-Development Site Conditions**

The proposed site improvements will include the construction of a new 45,000± SF storage building and a 10,000± building addition to their existing facility. Associated site improvements will include but not be limited to: new access driveways, parking areas for vehicles, sidewalks, landscaping, lighting, utilities, and stormwater management BMP's. An existing surface infiltration basin and new proposed underground infiltration system were design to attenuate stormwater discharge in the proposed site conditions and ensure that peak rates offsite are less than or equal to the existing site conditions.

Percolation test were conducted to determine the infiltration rate on site. Percolation test results indicated that the subsurface soil condition achieved an average perc rate of ~0.9 In/min or 54 in/hr. An infiltration rate of 27in/hr was used for the HydroCAD model for both infiltration areas considering a factor of safety of 2. See **Appendix B** for the Post Development Condition and Pond summary HydroCAD reports. The Proposed Conditions Drainage Map for the site can be found in **Appendix G**.

#### **Analysis of Results**

The pre-development and post-development conditions were analyzed using HydroCAD consistent with National Resource Conservation Service (NRCS) hydrology methods. One discharge location (**Design Point #1**) was identified as a point of interest for assessing downstream effects. The following table contains the data generated from the HydroCAD software:

Reach		2 year	10 year	25 year	50 year	100 year
DP#1 – Existing CB in King Street	Pre	4.12	13.42	20.47	25.94	32.32
	Post	3.77	13.38	20.47	25.67	32.31

As seen in the table above, storm events evaluated for the subject project will result in peak runoff rates in the proposed condition that are less than the peak runoff rates of the existing condition for 2-, 10-, 25-, 50- and 100-year design storms.

#### **Storm Sewer Collection System**

The proposed subsurface stormwater collection and conveyance system was designed to adequately convey proposed runoff under 10- year storm event conditions. The design of the storm sewers followed the guidelines set forth in the Connecticut Department of Transportation's Drainage Manual. It is estimated that during a 10-year storm event, all proposed subsurface culverts will convey storm runoff without resulting in any unacceptable flooding conditions. Storm Sewer calculation are included as **Appendix E** of this report.

#### **Water Quality**

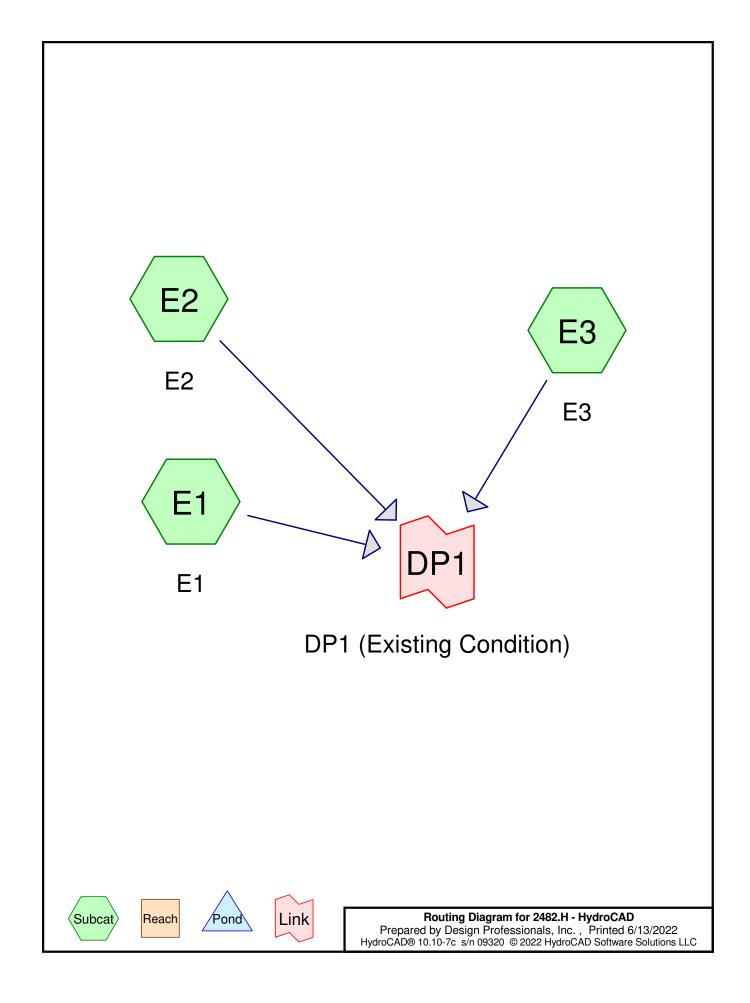
Stormtech Isolator rows will also be utilized to address water quality for all other areas draining to one of the proposed underground chamber systems and the two catchbasin to be located in the norther truck parking access drive. The number of isolator rows provided will be more than adequate to treat the required water quality flow rate based on the determined water quality flow and manufacture specs for

treated flow rate per chamber. The required water quality flow was also calculated considering recommended equations provided in the 2004 Connecticut Stormwater Quality Manual. Water Quality Flow calculations and isolation chamber specs are included as **Appendix F** of this report.

#### **Conclusion**

The proposed stormwater management system as discussed herein and shown on the referenced plans is appropriate for the proposed development on the subject site and should not pose any detrimental impacts to the environment.

# APPENDIX A Watershed Computations (Pre-Development Drainage HydroCAD Report)



Existing Condition Type III 24-hr 2-yr 24 hr Rainfall=3.08"

#### 2482.H - HydroCAD

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: E1 Runoff Area=241,775 sf 8.69% Impervious Runoff Depth=0.33"

Flow Length=735' Tc=32.2 min CN=59 Runoff=0.68 cfs 0.153 af

Subcatchment E2: E2 Runoff Area=395,349 sf 28.72% Impervious Runoff Depth=0.71"

Flow Length=936' Tc=53.4 min CN=69 Runoff=2.74 cfs 0.539 af

Subcatchment E3: E3 Runoff Area=111,153 sf 35.12% Impervious Runoff Depth=0.96"

Flow Length=1,158' Tc=19.7 min CN=74 Runoff=1.81 cfs 0.204 af

Link DP1: DP1 (Existing Condition) Inflow=4.12 cfs 0.896 af

Primary=4.12 cfs 0.896 af

Total Runoff Area = 17.178 ac Runoff Volume = 0.896 af Average Runoff Depth = 0.63" 76.80% Pervious = 13.193 ac 23.20% Impervious = 3.985 ac

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# Type III 24-hr 10-yr 24 hr Rainfall=4.88"

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: E1 Runoff Area=241,775 sf 8.69% Impervious Runoff Depth=1.17"

Flow Length=735' Tc=32.2 min CN=59 Runoff=3.63 cfs 0.540 af

Subcatchment E2: E2 Runoff Area=395,349 sf 28.72% Impervious Runoff Depth=1.87"

Flow Length=936' Tc=53.4 min CN=69 Runoff=8.14 cfs 1.415 af

Subcatchment E3: E3 Runoff Area=111,153 sf 35.12% Impervious Runoff Depth=2.27"

Flow Length=1,158' Tc=19.7 min CN=74 Runoff=4.56 cfs 0.482 af

Link DP1: DP1 (Existing Condition) Inflow=13.42 cfs 2.437 af

Primary=13.42 cfs 2.437 af

Total Runoff Area = 17.178 ac Runoff Volume = 2.437 af Average Runoff Depth = 1.70" 76.80% Pervious = 13.193 ac 23.20% Impervious = 3.985 ac

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Type III 24-hr 25-yr 24 hr Rainfall=6.01"

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: E1 Runoff Area=241,775 sf 8.69% Impervious Runoff Depth=1.85"

Flow Length=735' Tc=32.2 min CN=59 Runoff=6.14 cfs 0.853 af

Subcatchment E2: E2 Runoff Area=395,349 sf 28.72% Impervious Runoff Depth=2.72"

Flow Length=936' Tc=53.4 min CN=69 Runoff=12.07 cfs 2.057 af

Subcatchment E3: E3 Runoff Area=111,153 sf 35.12% Impervious Runoff Depth=3.19"

Flow Length=1,158' Tc=19.7 min CN=74 Runoff=6.47 cfs 0.679 af

Link DP1: DP1 (Existing Condition) Inflow=20.47 cfs 3.590 af

Primary=20.47 cfs 3.590 af

Total Runoff Area = 17.178 ac Runoff Volume = 3.590 af Average Runoff Depth = 2.51" 76.80% Pervious = 13.193 ac 23.20% Impervious = 3.985 ac

#### 2482.H - HydroCAD

Type III 24-hr 50-yr 24 hr Rainfall=6.83"

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: E1 Runoff Area=241,775 sf 8.69% Impervious Runoff Depth=2.39"

Flow Length=735' Tc=32.2 min CN=59 Runoff=8.15 cfs 1.105 af

Subcatchment E2: E2 Runoff Area=395,349 sf 28.72% Impervious Runoff Depth=3.38"

Flow Length=936' Tc=53.4 min CN=69 Runoff=15.07 cfs 2.553 af

Subcatchment E3: E3 Runoff Area=111,153 sf 35.12% Impervious Runoff Depth=3.89"

Flow Length=1,158' Tc=19.7 min CN=74 Runoff=7.90 cfs 0.828 af

Link DP1: DP1 (Existing Condition) Inflow=25.94 cfs 4.486 af

Primary=25.94 cfs 4.486 af

Total Runoff Area = 17.178 ac Runoff Volume = 4.486 af Average Runoff Depth = 3.13" 76.80% Pervious = 13.193 ac 23.20% Impervious = 3.985 ac

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# Type III 24-hr 100-yr 24 hr Rainfall=7.75"

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: E1 Runoff Area=241,775 sf 8.69% Impervious Runoff Depth=3.04"

Flow Length=735' Tc=32.2 min CN=59 Runoff=10.54 cfs 1.406 af

Subcatchment E2: E2 Runoff Area=395,349 sf 28.72% Impervious Runoff Depth=4.14"

Flow Length=936' Tc=53.4 min CN=69 Runoff=18.54 cfs 3.130 af

Subcatchment E3: E3 Runoff Area=111,153 sf 35.12% Impervious Runoff Depth=4.70"

Flow Length=1,158' Tc=19.7 min CN=74 Runoff=9.53 cfs 1.000 af

Link DP1: DP1 (Existing Condition) Inflow=32.32 cfs 5.535 af

Primary=32.32 cfs 5.535 af

Total Runoff Area = 17.178 ac Runoff Volume = 5.535 af Average Runoff Depth = 3.87" 76.80% Pervious = 13.193 ac 23.20% Impervious = 3.985 ac

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#### **Summary for Subcatchment E1: E1**

Runoff = 0.68 cfs @ 12.64 hrs, Volume= 0.153 a

0.153 af, Depth= 0.33"

Routed to Link DP1 : DP1 (Existing Condition)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Type III 24-hr 2-yr 24 hr Rainfall=3.08"

	Α	rea (sf)	CN E	escription		
		19,452				ood, HSG A
		5,573				ood, HSG B
*		21,019	98 II	MPERVIO	JS	
		1,467	30 N	leadow, no	on-grazed,	HSG A
	1	70,002			on-grazed,	
		29		•	on-grazed,	
		2,314			on-grazed,	HSG D
		4,974		•	od, HSG A	
		14,843		•	od, HSG B	
		1,962		•	od, HSG C	
_		140			od, HSG D	
		241,775		Veighted A		
		20,756	_		vious Area	
	21,019		8	.69% Impe	ervious Area	a
	т.	l	Olama	V-l!+	0	Description
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	OL 151 W 1 OF
	14.9	100	0.0520	0.11		Sheet Flow, Woods SF
	47.0	005	0.0450	0.04		Woods: Light underbrush n= 0.400 P2= 3.08"
	17.3	635	0.0150	0.61		Shallow Concentrated Flow, Woodland SCF
_		705	<b>-</b>			Woodland Kv= 5.0 fps
	32.2	735	Total			

# **Summary for Subcatchment E2: E2**

Runoff = 2.74 cfs @ 12.82 hrs, Volume= 0.539 af, Depth= 0.71" Routed to Link DP1 : DP1 (Existing Condition)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Type III 24-hr 2-yr 24 hr Rainfall=3.08"

	Area (sf)	CN	Description
	44,072	61	>75% Grass cover, Good, HSG B
*	113,537	98	IMPERVIOUS
	165,668	58	Meadow, non-grazed, HSG B
	72,072	55	Woods, Good, HSG B
	395,349	69	Weighted Average
	281,812		71.28% Pervious Area
	113,537		28.72% Impervious Area

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_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	31.6	100	0.0080	0.05		Sheet Flow, Woods SF
	21.1	491	0.0060	0.39		Woods: Light underbrush n= 0.400 P2= 3.08" <b>Shallow Concentrated Flow, Woodland SCF</b>
						Woodland Kv= 5.0 fps
	0.7	345	0.0050	8.01	77.07	Pipe Channel, 42IN RCP
						42.0" Round Area= 9.6 sf Perim= 11.0' r= 0.88'
_						n= 0.012 Concrete pipe, finished
	53.4	936	Total			

#### **Summary for Subcatchment E3: E3**

Runoff = 1.81 cfs @ 12.30 hrs, Volume= 0.2

0.204 af, Depth= 0.96"

Routed to Link DP1 : DP1 (Existing Condition)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Type III 24-hr 2-yr 24 hr Rainfall=3.08"

	Α	rea (sf)	CN [	Description		
		20,028	61 >	75% Gras	s cover, Go	ood, HSG B
		144	80 >	-75% Gras	s cover, Go	ood, HSG D
*		39,039	98 I	MPERVIO	US	
		22,144	58 N	Meadow, no	on-grazed,	HSG B
		4,229	78 <b>N</b>	Meadow, no	on-grazed,	HSG D
		18,305	55 \	Voods, Go	od, HSG B	
		7,264	77 <b>\</b>	Voods, Go	od, HSG D	
	1	11,153	74 \	Veighted A	verage	
		72,114	6	64.88% Pe	rvious Area	
		39,039	3	35.12% lmp	pervious Ar	ea
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	13.3	100	0.0250	0.13		Sheet Flow, Grass SF
						Grass: Dense n= 0.240 P2= 3.08"
	4.7	1,008	0.0310	3.57		Shallow Concentrated Flow, Paved SCF
						Paved Kv= 20.3 fps
	0.7	50	0.0310	1.23		Shallow Concentrated Flow, Grass SCF
						Short Grass Pasture Kv= 7.0 fps
	1.0					Direct Entry, Pipe flow to Design Point (approx)
	19.7	1,158	Total			

#### **Summary for Link DP1: DP1 (Existing Condition)**

Inflow Area = 17.178 ac, 23.20% Impervious, Inflow Depth = 0.63" for 2-yr 24 hr event

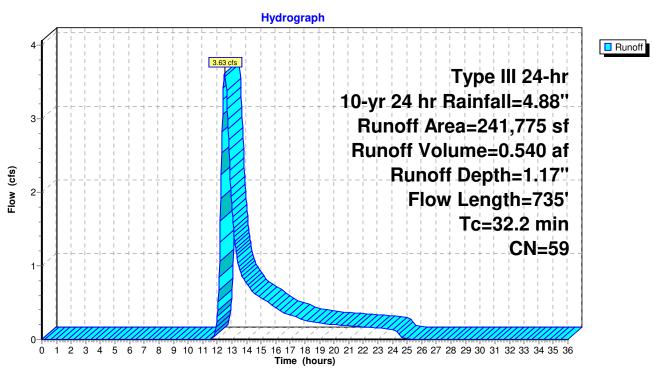
Inflow = 4.12 cfs @ 12.67 hrs, Volume= 0.896 af

Primary = 4.12 cfs @ 12.67 hrs, Volume= 0.896 af, Atten= 0%, Lag= 0.0 min

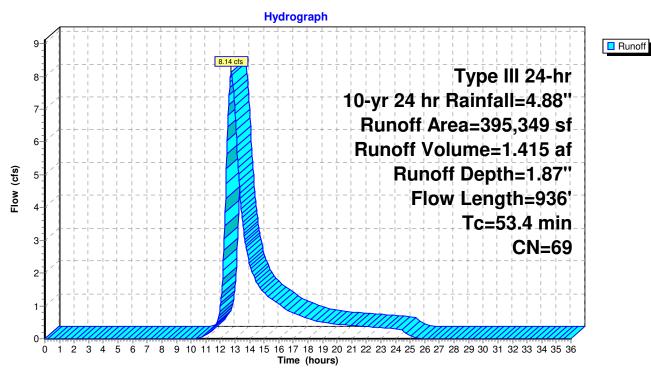
Primary outflow = Inflow, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs

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Subcatchment E1: E1

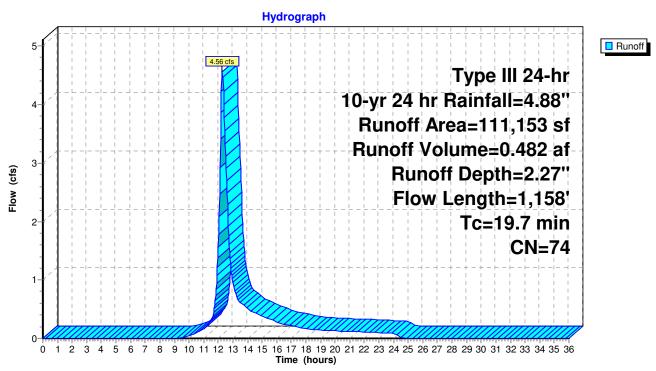


#### **Subcatchment E2: E2**

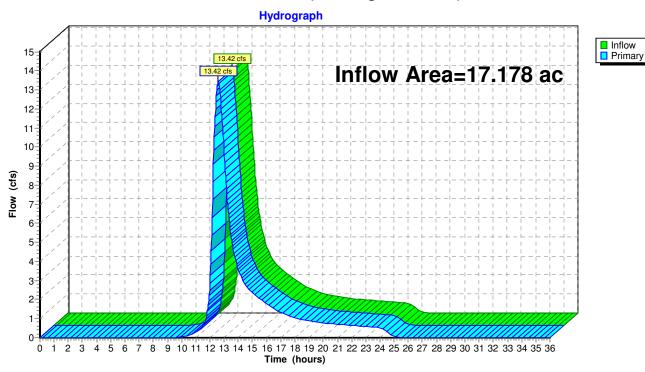


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Subcatchment E3: E3



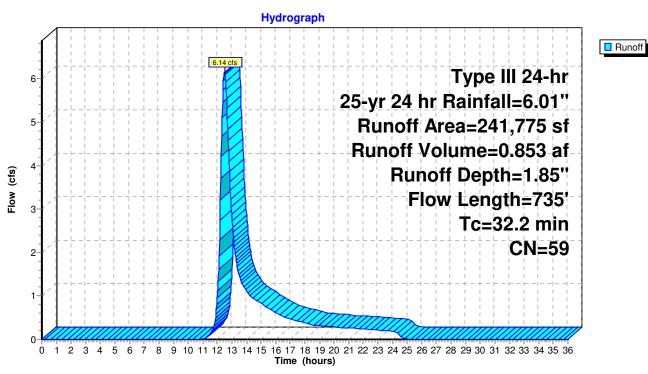
### **Link DP1: DP1 (Existing Condition)**



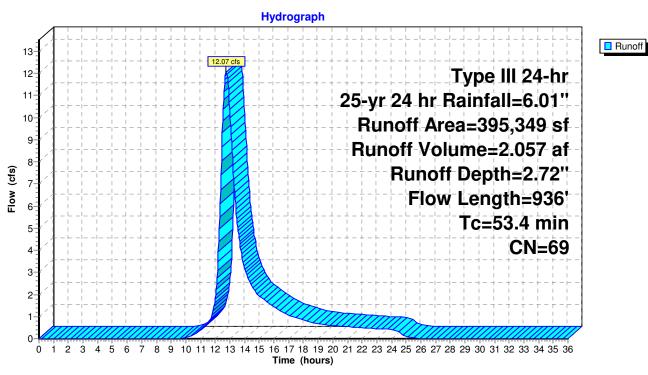
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Subcatchment E1: E1

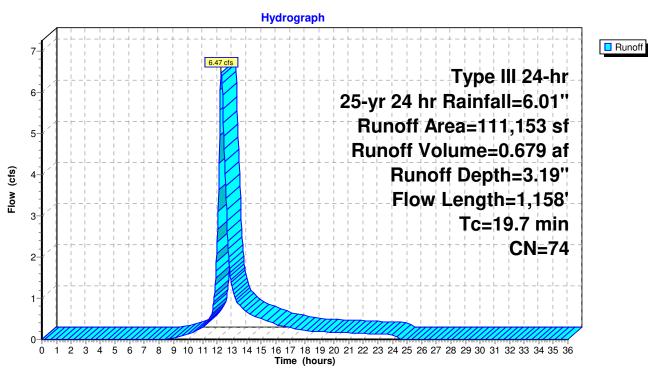


#### Subcatchment E2: E2

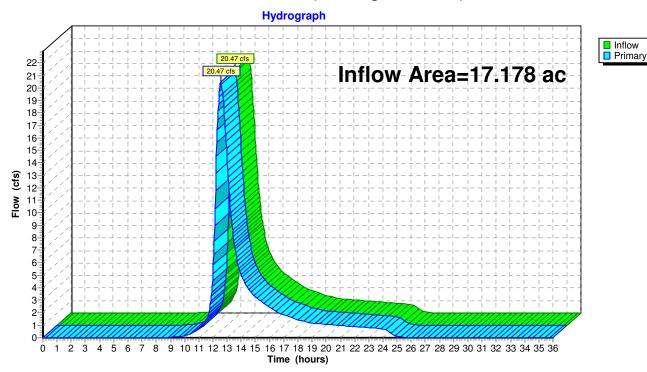


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#### Subcatchment E3: E3

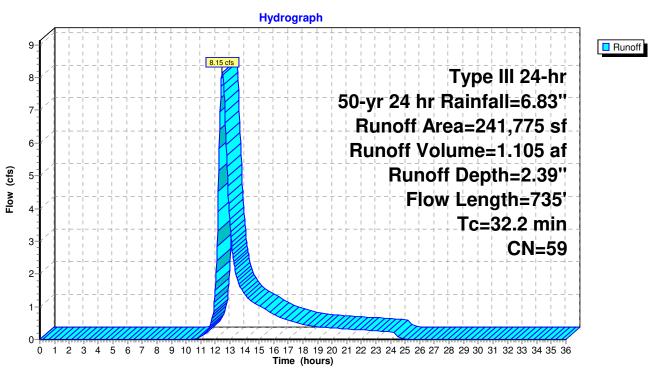


### **Link DP1: DP1 (Existing Condition)**

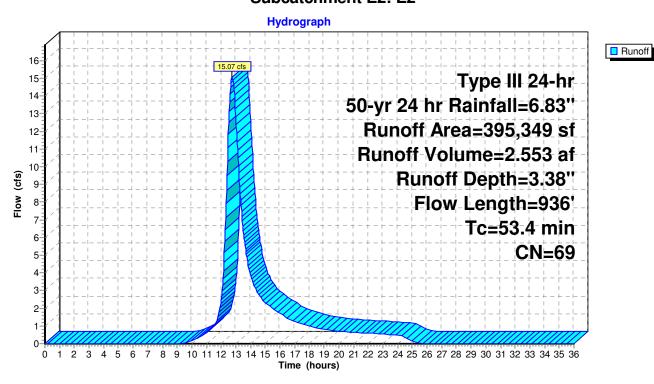


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Subcatchment E1: E1



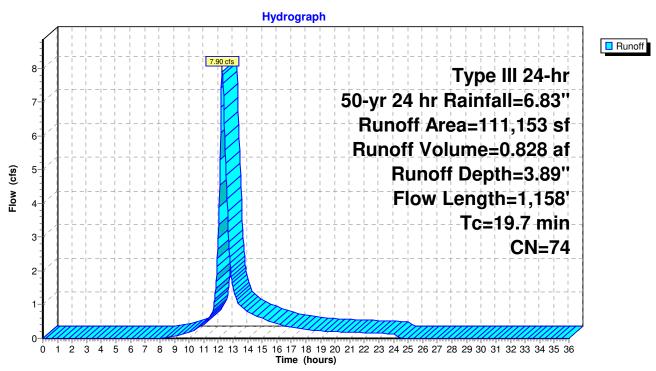
#### Subcatchment E2: E2



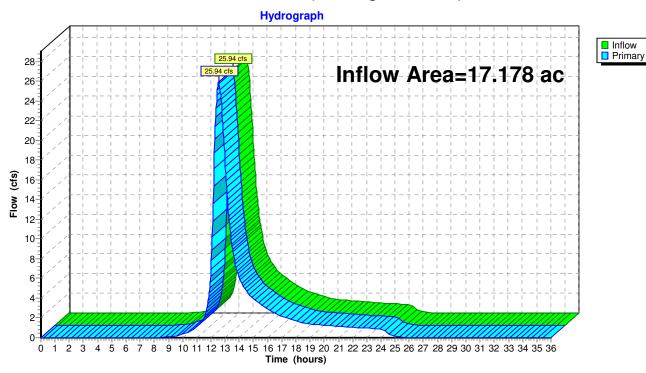
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#### Subcatchment E3: E3



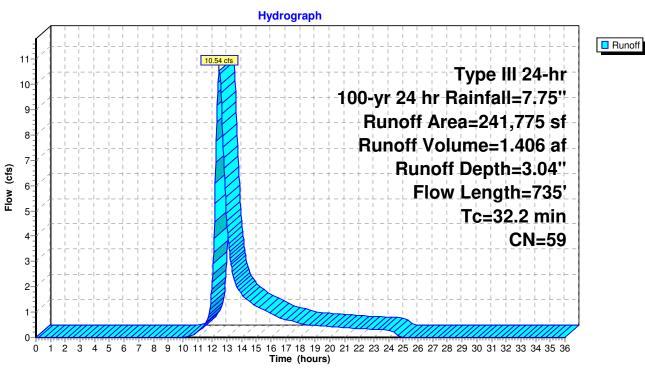
#### **Link DP1: DP1 (Existing Condition)**



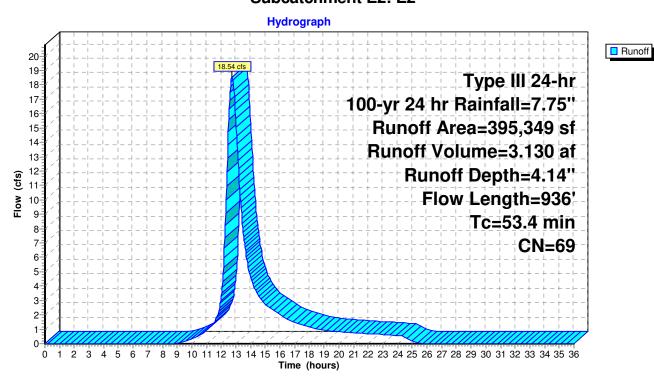
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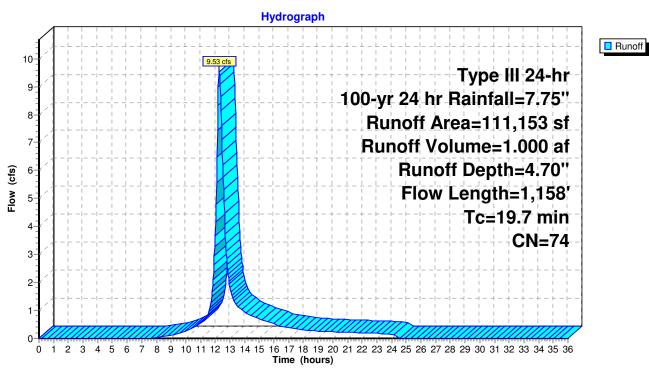
#### Subcatchment E1: E1



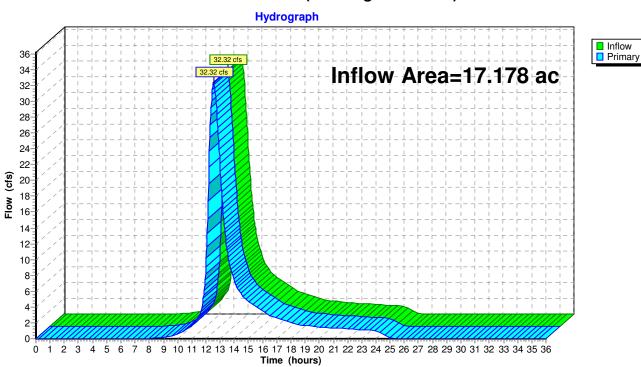
#### Subcatchment E2: E2



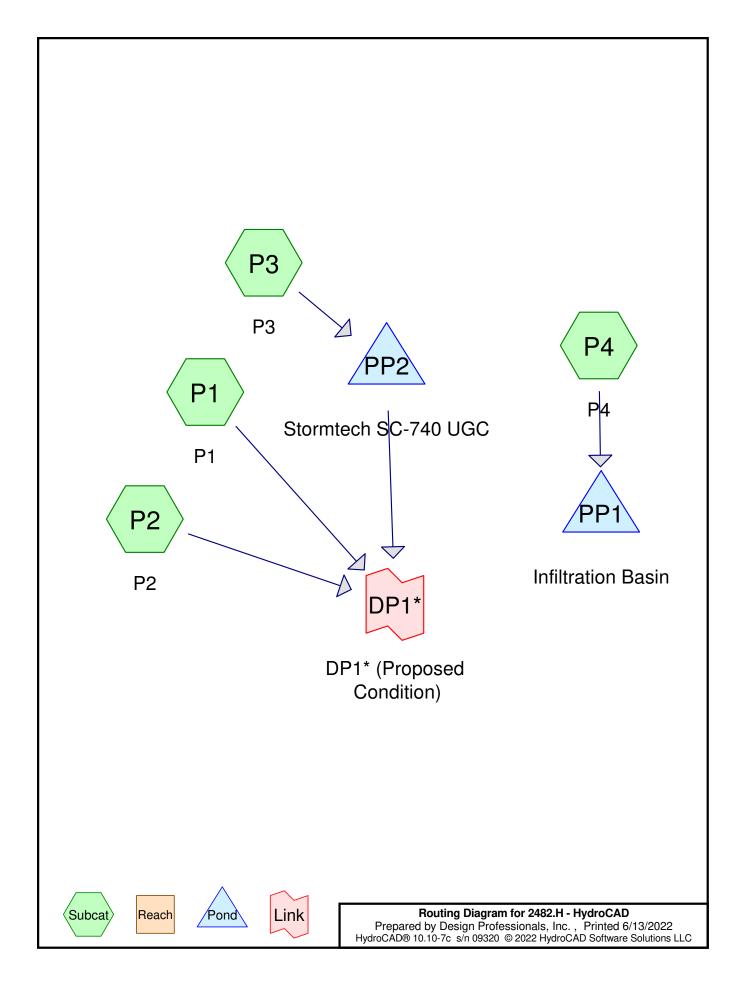
#### Subcatchment E3: E3



#### **Link DP1: DP1 (Existing Condition)**



# APPENDIX B Watershed Computations (Post-Development Drainage HydroCAD Report)



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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: P1 Runoff Area=100,066 sf 20.78% Impervious Runoff Depth=0.47"

Flow Length=642' Tc=17.2 min CN=63 Runoff=0.61 cfs 0.089 af

Subcatchment P2: P2 Runoff Area=252,718 sf 44.93% Impervious Runoff Depth=1.07"

Flow Length=351' Slope=0.0080 '/' Tc=42.0 min CN=76 Runoff=3.34 cfs 0.517 af

Subcatchment P3: P3 Runoff Area=383,881 sf 83.39% Impervious Runoff Depth=2.24"

Tc=20.0 min CN=92 Runoff=15.31 cfs 1.643 af

Subcatchment P4: P4 Runoff Area=121,706 sf 36.85% Impervious Runoff Depth=1.01"

Tc=8.0 min CN=75 Runoff=2.93 cfs 0.236 af

Pond PP1: Infiltration Basin Peak Elev=46.71' Storage=1,016 cf Inflow=2.93 cfs 0.236 af

Outflow=1.93 cfs 0.236 af

Pond PP2: Stormtech SC-740 UGC Peak Elev=44.63' Storage=3,855 cf Inflow=15.31 cfs 1.643 af

Discarded=10.71 cfs 1.643 af Primary=0.00 cfs 0.000 af Outflow=10.72 cfs 1.643 af

Link DP1\*: DP1\* (Proposed Condition) Inflow=3.77 cfs 0.606 af

Primary=3.77 cfs 0.606 af

Total Runoff Area = 19.705 ac Runoff Volume = 2.485 af Average Runoff Depth = 1.51" 41.83% Pervious = 8.243 ac 58.17% Impervious = 11.462 ac

Proposed Condition Type III 24-hr 10-yr 24 hr Rainfall=4.88"

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: P1 Runoff Area=100,066 sf 20.78% Impervious Runoff Depth=1.43"

Flow Length=642' Tc=17.2 min CN=63 Runoff=2.54 cfs 0.274 af

Subcatchment P2: P2 Runoff Area=252,718 sf 44.93% Impervious Runoff Depth=2.44"

Flow Length=351' Slope=0.0080 '/' Tc=42.0 min CN=76 Runoff=7.92 cfs 1.178 af

Subcatchment P3: P3 Runoff Area=383,881 sf 83.39% Impervious Runoff Depth=3.97"

Tc=20.0 min CN=92 Runoff=26.49 cfs 2.917 af

Subcatchment P4: P4 Runoff Area=121,706 sf 36.85% Impervious Runoff Depth=2.35"

Tc=8.0 min CN=75 Runoff=7.13 cfs 0.548 af

Pond PP1: Infiltration Basin Peak Elev=47.23' Storage=3,801 cf Inflow=7.13 cfs 0.548 af

Outflow=3.19 cfs 0.548 af

Pond PP2: Stormtech SC-740 UGC Peak Elev=45.53' Storage=16,407 cf Inflow=26.49 cfs 2.917 af

Discarded=11.01 cfs 2.752 af Primary=3.95 cfs 0.165 af Outflow=14.96 cfs 2.917 af

Link DP1\*: DP1\* (Proposed Condition) Inflow=13.38 cfs 1.618 af

Primary=13.38 cfs 1.618 af

Total Runoff Area = 19.705 ac Runoff Volume = 4.917 af Average Runoff Depth = 2.99" 41.83% Pervious = 8.243 ac 58.17% Impervious = 11.462 ac

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: P1 Runoff Area=100,066 sf 20.78% Impervious Runoff Depth=2.18"

Flow Length=642' Tc=17.2 min CN=63 Runoff=4.05 cfs 0.418 af

Subcatchment P2: P2 Runoff Area=252,718 sf 44.93% Impervious Runoff Depth=3.39"

Flow Length=351' Slope=0.0080 '/' Tc=42.0 min CN=76 Runoff=11.07 cfs 1.638 af

Subcatchment P3: P3 Runoff Area=383,881 sf 83.39% Impervious Runoff Depth=5.08"

Tc=20.0 min CN=92 Runoff=33.44 cfs 3.730 af

Subcatchment P4: P4 Runoff Area=121,706 sf 36.85% Impervious Runoff Depth=3.29"

Tc=8.0 min CN=75 Runoff=10.01 cfs 0.766 af

Pond PP1: Infiltration Basin Peak Elev=47.51' Storage=7,124 cf Inflow=10.01 cfs 0.766 af

Outflow=3.19 cfs 0.766 af

Pond PP2: Stormtech SC-740 UGC Peak Elev=46.14' Storage=24,081 cf Inflow=33.44 cfs 3.730 af

Discarded=11.21 cfs 3.347 af Primary=7.11 cfs 0.384 af Outflow=18.31 cfs 3.730 af

Link DP1\*: DP1\* (Proposed Condition) Inflow=20.47 cfs 2.440 af

Primary=20.47 cfs 2.440 af

Total Runoff Area = 19.705 ac Runoff Volume = 6.553 af Average Runoff Depth = 3.99" 41.83% Pervious = 8.243 ac 58.17% Impervious = 11.462 ac

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: P1 Runoff Area=100,066 sf 20.78% Impervious Runoff Depth=2.77"

Flow Length=642' Tc=17.2 min CN=63 Runoff=5.23 cfs 0.531 af

Subcatchment P2: P2 Runoff Area=252,718 sf 44.93% Impervious Runoff Depth=4.11"

Flow Length=351' Slope=0.0080 '/' Tc=42.0 min CN=76 Runoff=13.41 cfs 1.985 af

Subcatchment P3: P3 Runoff Area=383,881 sf 83.39% Impervious Runoff Depth=5.89"

Tc=20.0 min CN=92 Runoff=38.45 cfs 4.323 af

Subcatchment P4: P4 Runoff Area=121,706 sf 36.85% Impervious Runoff Depth=4.00"

Tc=8.0 min CN=75 Runoff=12.17 cfs 0.931 af

Pond PP1: Infiltration Basin Peak Elev=47.69' Storage=9,926 cf Inflow=12.17 cfs 0.931 af

Outflow=3.19 cfs 0.931 af

Pond PP2: Stormtech SC-740 UGC Peak Elev=46.66' Storage=29,850 cf Inflow=38.45 cfs 4.323 af

Discarded=11.38 cfs 3.757 af Primary=9.38 cfs 0.567 af Outflow=20.75 cfs 4.323 af

Link DP1\*: DP1\* (Proposed Condition) Inflow=25.67 cfs 3.083 af

Primary=25.67 cfs 3.083 af

Total Runoff Area = 19.705 ac Runoff Volume = 7.771 af Average Runoff Depth = 4.73" 41.83% Pervious = 8.243 ac 58.17% Impervious = 11.462 ac

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Time span=0.00-36.00 hrs, dt=0.03 hrs, 1201 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: P1 Runoff Area=100,066 sf 20.78% Impervious Runoff Depth=3.47"

Flow Length=642' Tc=17.2 min CN=63 Runoff=6.62 cfs 0.665 af

Subcatchment P2: P2 Runoff Area=252,718 sf 44.93% Impervious Runoff Depth=4.93"

Flow Length=351' Slope=0.0080 '/' Tc=42.0 min CN=76 Runoff=16.07 cfs 2.384 af

Subcatchment P3: P3 Runoff Area=383,881 sf 83.39% Impervious Runoff Depth=6.80"

Tc=20.0 min CN=92 Runoff=44.05 cfs 4.991 af

Subcatchment P4: P4 Runoff Area=121,706 sf 36.85% Impervious Runoff Depth=4.82"

Tc=8.0 min CN=75 Runoff=14.61 cfs 1.121 af

Pond PP1: Infiltration Basin Peak Elev=47.87' Storage=13,346 cf Inflow=14.61 cfs 1.121 af

Outflow=3.19 cfs 1.121 af

Pond PP2: Stormtech SC-740 UGC Peak Elev=47.44' Storage=35,782 cf Inflow=44.05 cfs 4.991 af

Discarded=11.63 cfs 4.193 af Primary=12.61 cfs 0.798 af Outflow=24.25 cfs 4.991 af

Link DP1\*: DP1\* (Proposed Condition) Inflow=32.31 cfs 3.847 af

Primary=32.31 cfs 3.847 af

Total Runoff Area = 19.705 ac Runoff Volume = 9.161 af Average Runoff Depth = 5.58" 41.83% Pervious = 8.243 ac 58.17% Impervious = 11.462 ac

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#### **Summary for Subcatchment P1: P1**

Runoff = 0.61 cfs @ 12.33 hrs, Volume=

0.089 af, Depth= 0.47"

Routed to Link DP1\*: DP1\* (Proposed Condition)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Type III 24-hr 2-yr 24 hr Rainfall=3.08"

A	Area (sf)	CN E	Description		
	23,422	39 >	75% Gras	s cover, Go	ood, HSG A
	43,628				ood, HSG B
	636	74 >	75% Gras	s cover, Go	ood, HSG C
*	20,798	98 II	<b>MPERVIO</b> I	JS	
	45	30 N	/leadow, no	on-grazed,	HSG A
	2,031	58 N	/leadow, no	on-grazed,	HSG B
	14	71 N	/leadow, no	on-grazed,	HSG C
	2,448	30 V	Voods, Go	od, HSG A	
	5,704	55 V	Voods, Go	od, HSG B	
	1,340	70 V	Voods, Go	od, HSG C	
•	100,066	63 V	Veighted A	verage	
	79,268	7	'9.22% Per	vious Area	
	20,798	2	0.78% Imp	ervious Ar	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
12.9	100	0.0271	0.13		Sheet Flow, Grass SF
					Grass: Dense n= 0.240 P2= 3.08"
4.3	542	0.0200	2.12		Shallow Concentrated Flow, Woodland SCF
					Grassed Waterway Kv= 15.0 fps
17.2	642	Total	·	·	

# **Summary for Subcatchment P2: P2**

Runoff = 3.34 cfs @ 12.62 hrs, Volume=

0.517 af, Depth= 1.07"

Routed to Link DP1\*: DP1\* (Proposed Condition)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Type III 24-hr 2-yr 24 hr Rainfall=3.08"

	Area (sf)	CN	Description
	80,731	61	>75% Grass cover, Good, HSG B
*	113,537	98	IMPERVIOUS
	3,913	58	Meadow, non-grazed, HSG B
	54,537	55	Woods, Good, HSG B
	252,718	76	Weighted Average
	139,181		55.07% Pervious Area
	113,537		44.93% Impervious Area

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	Tc	Length	Slope	,	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	31.6	100	0.0080	0.05		Sheet Flow, Woodland SF
						Woods: Light underbrush n= 0.400 P2= 3.08"
	9.4	251	0.0080	0.45		Shallow Concentrated Flow, Woodland
						Woodland Kv= 5.0 fps
	1.0					Direct Entry, Pipe flow to Design Point (approx)
_	42.0	351	Total			

#### **Summary for Subcatchment P3: P3**

Runoff = 15.31 cfs @ 12.27 hrs, Volume=

1.643 af, Depth= 2.24"

Routed to Pond PP2: Stormtech SC-740 UGC

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Type III 24-hr 2-yr 24 hr Rainfall=3.08"

	Ar	rea (sf)	CN	Description			
		39,771	61	>75% Gras	s cover, Go	ood, HSG B	
		6,221	80	>75% Gras	s cover, Go	ood, HSG D	
*	3	20,105	98	<b>IMPERVIO</b>	JS		
		17,575	55	Woods, Go	od, HSG B		
		209	77	Woods, Go	od, HSG D		
	3	83,881	92	Weighted A	verage		
		63,776		16.61% Per	vious Area	A	
	3	20,105		83.39% Imp	pervious Ar	rea	
	Tc	Length	Slop		Capacity	Description	
(r	nin)	(feet)	(ft/f	(ft/sec)	(cfs)		
2	20.0					Direct Entry,	

# **Summary for Subcatchment P4: P4**

Runoff = 2.93 cfs @ 12.12 hrs, Volume=

0.236 af, Depth= 1.01"

Routed to Pond PP1: Infiltration Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Type III 24-hr 2-yr 24 hr Rainfall=3.08"

	Area (sf)	CN	Description
	76,856	61	>75% Grass cover, Good, HSG B
*	44,850	98	IMPERVIOUS
	121,706	75	Weighted Average
	76,856		63.15% Pervious Area
	44,850		36.85% Impervious Area

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	•	•	•		Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.0					Direct Entry,

#### **Summary for Pond PP1: Infiltration Basin**

#### \*No infiltration accounted for in Volume #2

Inflow Area = 2.794 ac, 36.85% Impervious, Inflow Depth = 1.01" for 2-yr 24 hr event

Inflow = 2.93 cfs @ 12.12 hrs, Volume= 0.236 af

Outflow = 1.93 cfs @ 12.25 hrs, Volume= 0.236 af, Atten= 34%, Lag= 7.8 min

Discarded = 1.93 cfs @ 12.25 hrs, Volume= 0.236 af

Doubling by Star lad method Time Span 0.00.26.00 bro. dt 0.02 bro.

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Peak Elev= 46.71' @ 12.25 hrs Surf.Area= 3,087 sf Storage= 1,016 cf

Plug-Flow detention time= 4.1 min calculated for 0.236 af (100% of inflow)

Center-of-Mass det. time= 4.1 min (867.1 - 863.0)

Volume	Invert	Avail.Storage	Storage Description
#1	46.00'	2,189 cf	Custom Stage Data (Conic) Listed below (Recalc)
#2	47.00'	77,493 cf	Custom Stage Data (Prismatic) Listed below (Recalc) -Impervious
		79,682 cf	Total Available Storage

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
46.00	277	0	0	277
47.00	5,101	2,189	2,189	5,104
Elevation (feet)	Surf.Area (sg-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
47.00	5,101	0	0	
48.00	22,964	14,033	14,033	
49.00	27,625	25,295	39,327	
50.00	48,707	38,166	77,493	

#1	Discarded		27.000 in/hr Exfiltration over Wetted area	
Device	Routing	Invert	Outlet Devices	

**Discarded OutFlow** Max=1.93 cfs @ 12.25 hrs HW=46.71' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 1.93 cfs)

# Summary for Pond PP2: Stormtech SC-740 UGC

Top of Pond 47.6

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Inflow Area =	8.813 ac, 83.39% Impervious, Inflow	Depth = 2.24" for 2-yr 24 hr event
Inflow =	15.31 cfs @ 12.27 hrs, Volume=	1.643 af
Outflow =	10.72 cfs @ 12.47 hrs, Volume=	1.643 af, Atten= 30%, Lag= 12.3 min
Discarded =	10.71 cfs @ 12.47 hrs, Volume=	1.643 af
Primary =	0.00 cfs @ 12.47 hrs, Volume=	0.000 af
Routed to Link	CDP1*: DP1* (Proposed Condition)	

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Peak Elev= 44.63' @ 12.47 hrs Surf.Area= 16,865 sf Storage= 3,855 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 1.5 min (813.7 - 812.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	44.10'	14,790 cf	115.50'W x 146.02'L x 3.50'H Field A
			59,027 cf Overall - 22,051 cf Embedded = 36,976 cf x 40.0% Voids
#2A	44.60'	22,051 cf	ADS_StormTech SC-740 +Cap x 480 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			480 Chambers in 24 Rows
		36,842 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	44.10'	27.000 in/hr Exfiltration over Wetted area
#2	Primary	44.61'	24.0" Round Culvert
			L= 29.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 44.61' / 44.32' S= 0.0100 '/' Cc= 0.900
			n= 0.012 Corrugated PP, smooth interior, Flow Area= 3.14 sf
#3	Device 2	44.61'	<b>34.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads
#4	Device 2	45.55'	<b>21.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads
#5	Device 2	46.40'	<b>12.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads

**Discarded OutFlow** Max=10.71 cfs @ 12.47 hrs HW=44.63' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 10.71 cfs)

Primary OutFlow Max=0.00 cfs @ 12.47 hrs HW=44.63' (Free Discharge)

2=Culvert (Barrel Controls 0.00 cfs @ 0.63 fps)

3=Orifice/Grate (Passes 0.00 cfs of 0.03 cfs potential flow)

-4=Orifice/Grate (Controls 0.00 cfs) -5=Orifice/Grate (Controls 0.00 cfs)

Proposed Condition Type III 24-hr 2-yr 24 hr Rainfall=3.08"

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# **Summary for Link DP1\*: DP1\* (Proposed Condition)**

Inflow Area = 16.912 ac, 61.69% Impervious, Inflow Depth = 0.43" for 2-yr 24 hr event

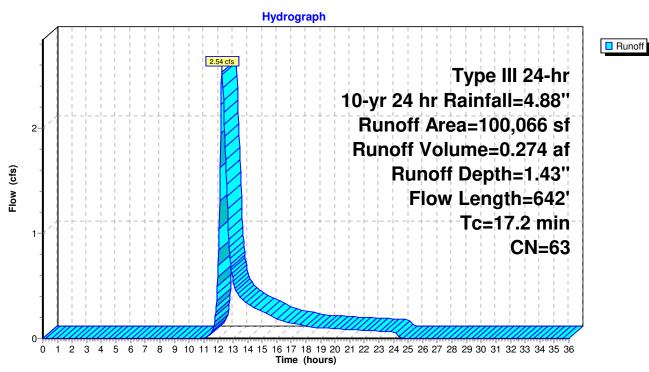
Inflow = 3.77 cfs @ 12.58 hrs, Volume= 0.606 af

Primary = 3.77 cfs @ 12.58 hrs, Volume= 0.606 af, Atten= 0%, Lag= 0.0 min

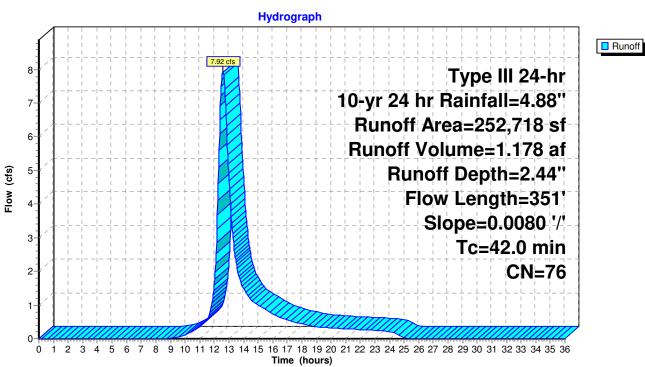
Primary outflow = Inflow, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs

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#### Subcatchment P1: P1



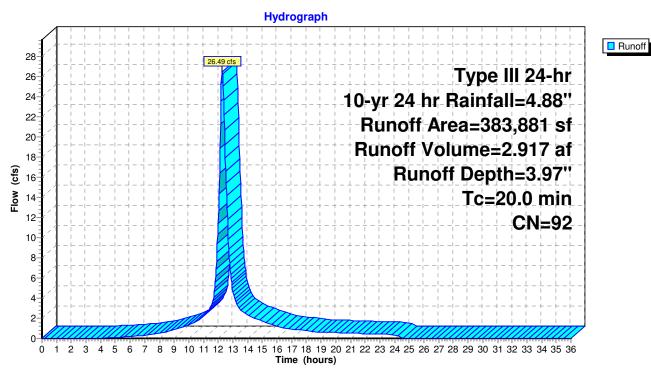
#### **Subcatchment P2: P2**



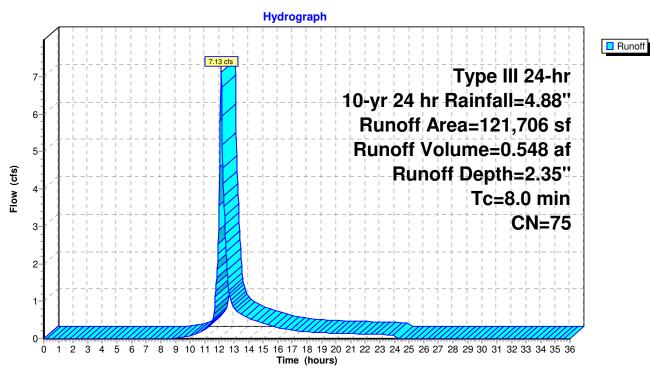
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#### Subcatchment P3: P3

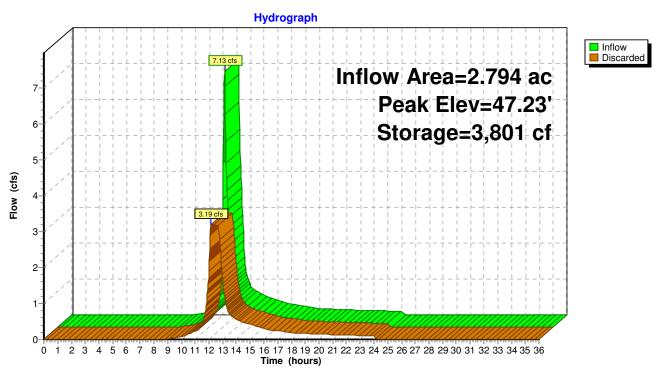


#### **Subcatchment P4: P4**

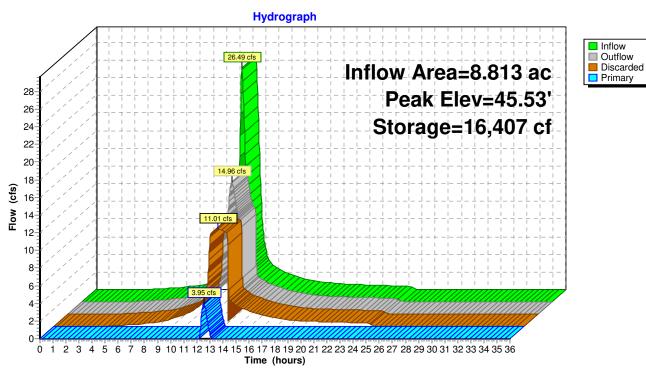


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#### **Pond PP1: Infiltration Basin**

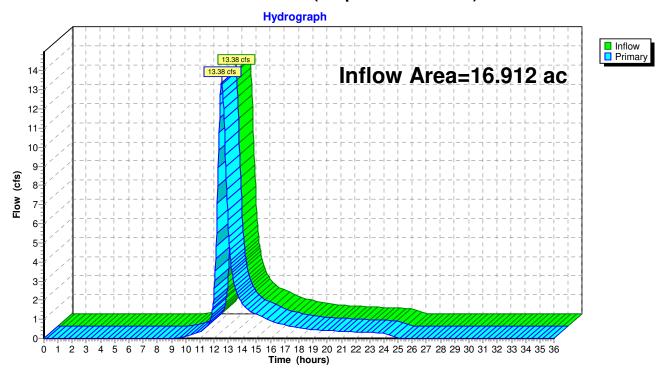


#### Pond PP2: Stormtech SC-740 UGC



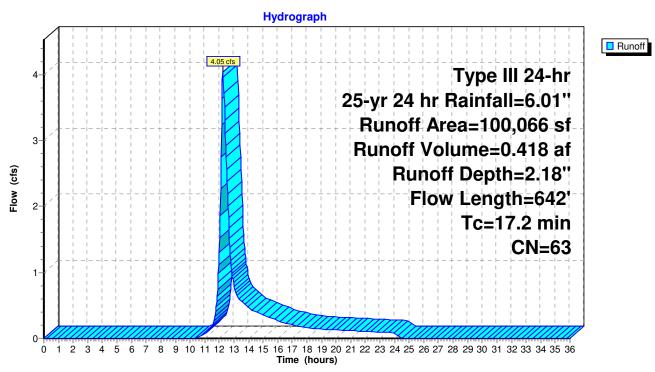
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# **Link DP1\*: DP1\* (Proposed Condition)**

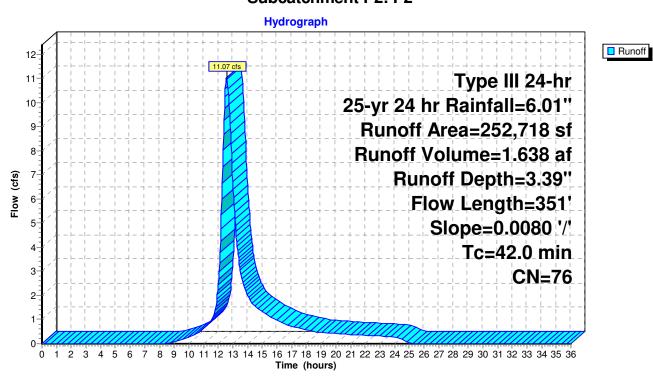


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#### **Subcatchment P1: P1**



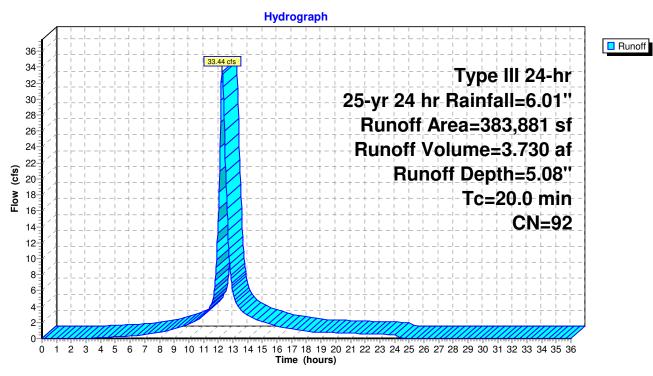
#### Subcatchment P2: P2



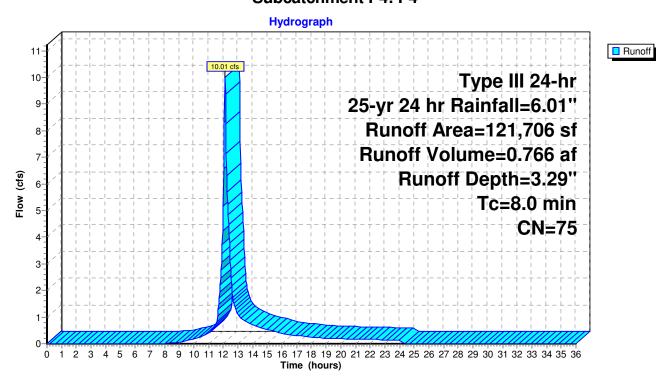
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#### **Subcatchment P3: P3**

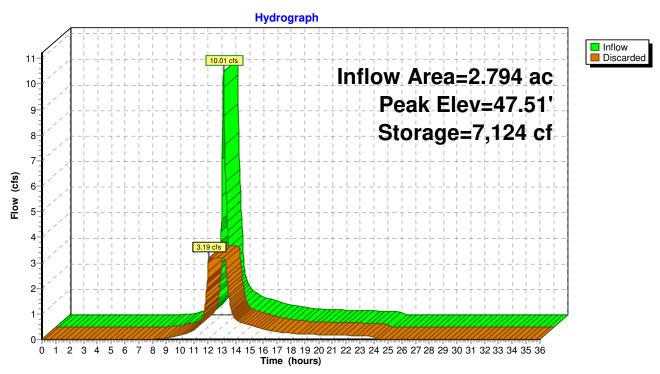


#### **Subcatchment P4: P4**

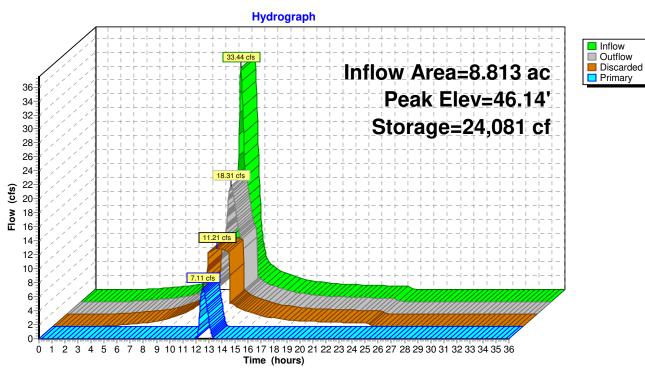


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#### **Pond PP1: Infiltration Basin**



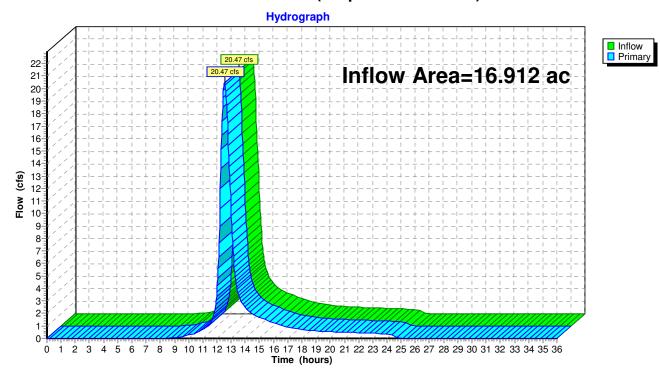
#### Pond PP2: Stormtech SC-740 UGC



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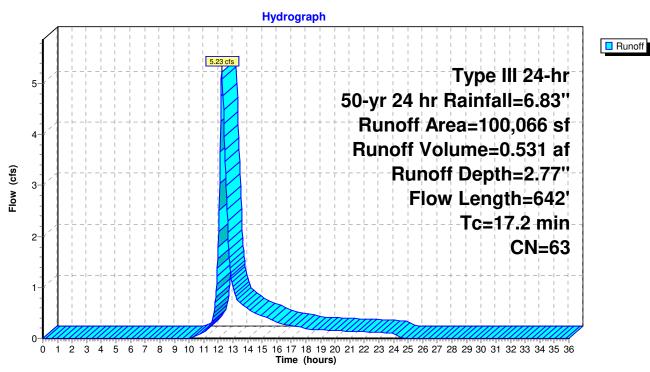
# **Link DP1\*: DP1\* (Proposed Condition)**



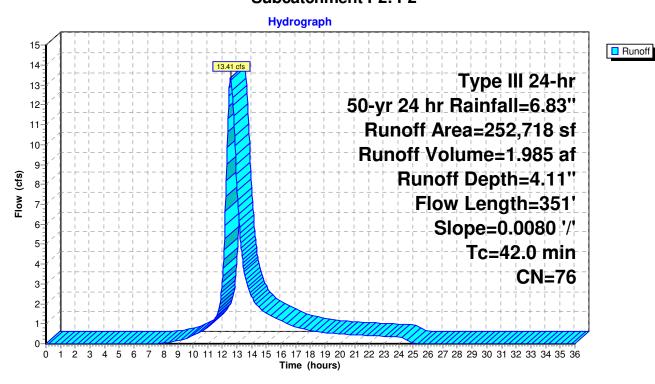
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#### **Subcatchment P1: P1**



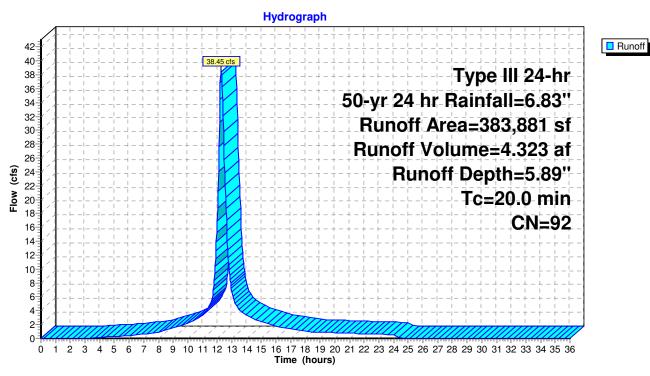
#### **Subcatchment P2: P2**



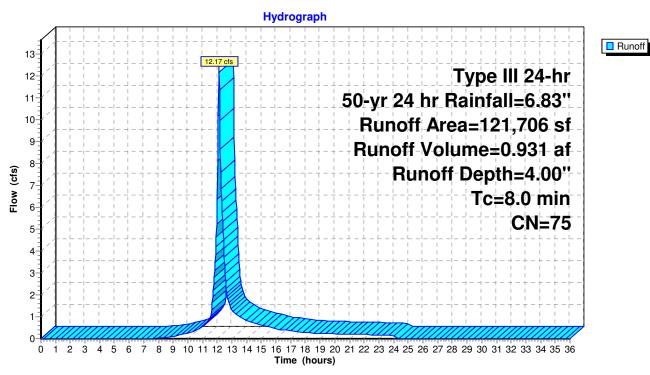
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**Subcatchment P3: P3** 



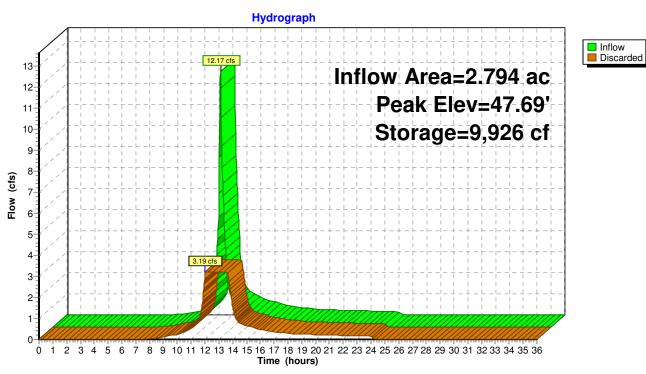
#### **Subcatchment P4: P4**



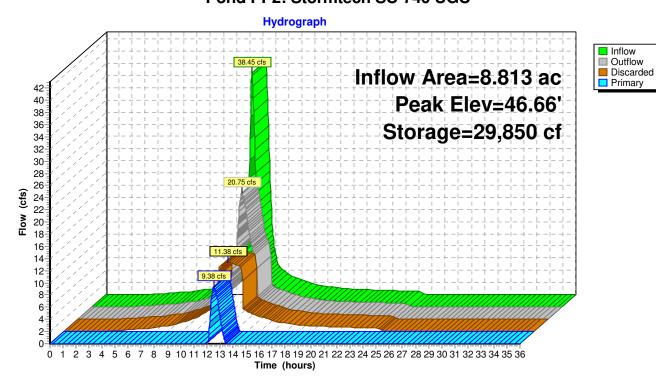
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#### **Pond PP1: Infiltration Basin**

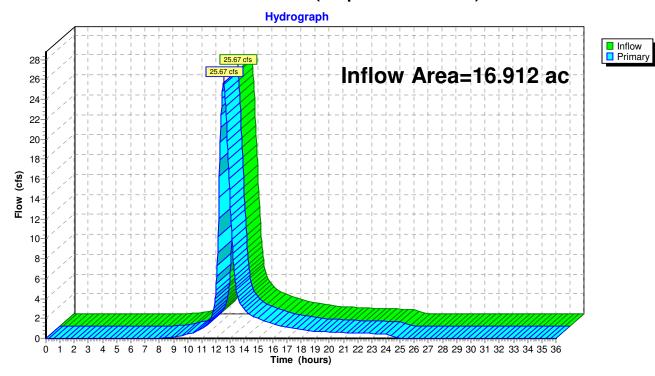


#### Pond PP2: Stormtech SC-740 UGC



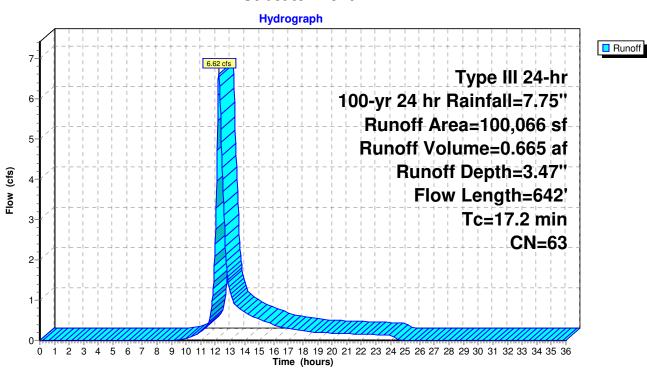
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# **Link DP1\*: DP1\* (Proposed Condition)**

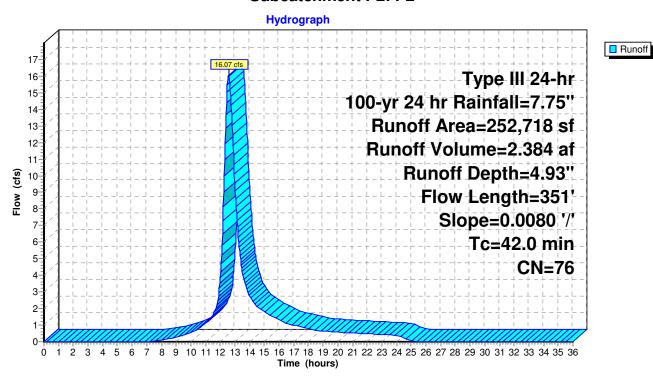


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Subcatchment P1: P1



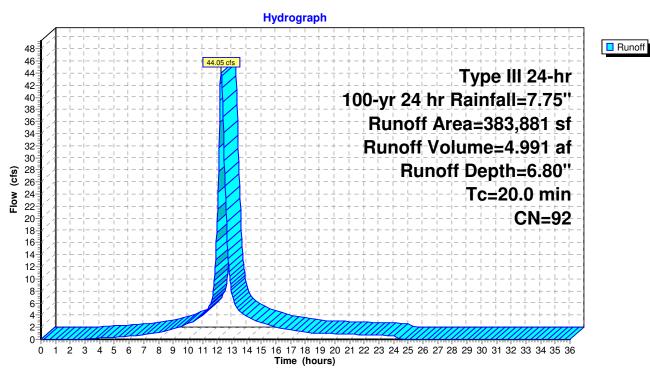
#### Subcatchment P2: P2



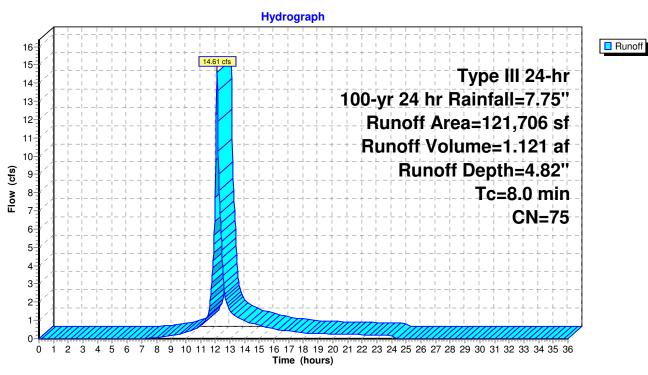
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Subcatchment P3: P3

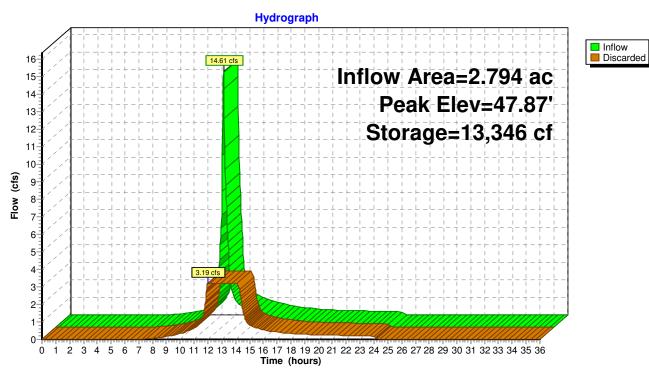


#### Subcatchment P4: P4

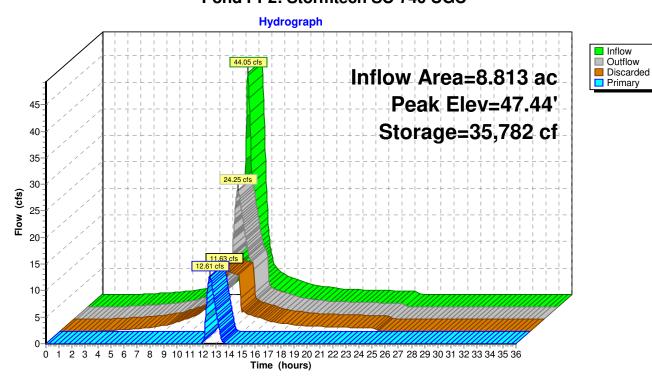


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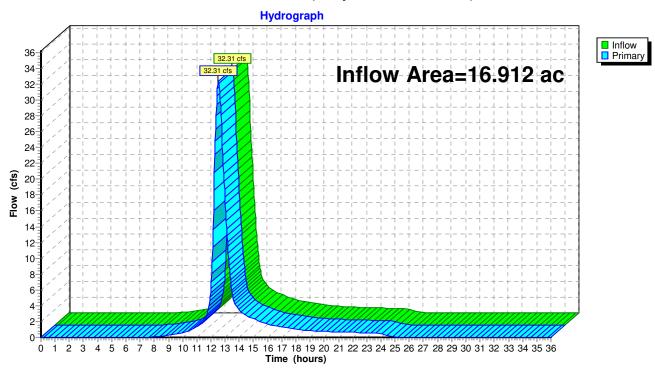
#### **Pond PP1: Infiltration Basin**



#### Pond PP2: Stormtech SC-740 UGC



# **Link DP1\*: DP1\* (Proposed Condition)**



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### **Summary for Pond PP1: Infiltration Basin**

#### \*No infiltration accounted for in Volume #2

Inflow Area = 2.794 ac, 36.85% Impervious, Inflow Depth = 4.82" for 100-yr 24 hr event

Inflow = 14.61 cfs @ 12.11 hrs, Volume= 1.121 af

Outflow = 3.19 cfs @ 11.97 hrs, Volume= 1.121 af, Atten= 78%, Lag= 0.0 min

Discarded = 3.19 cfs @ 11.97 hrs, Volume= 1.121 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Peak Elev= 47.87' @ 12.56 hrs Surf.Area= 5,101 sf Storage= 13,346 cf

Plug-Flow detention time= 26.9 min calculated for 1.121 af (100% of inflow)

Center-of-Mass det. time= 26.9 min (844.2 - 817.3)

Volume	Invert	Avail.Storage	Storage Description
#1	46.00'	2,189 cf	Custom Stage Data (Conic) Listed below (Recalc)
#2	47.00'	77,493 cf	Custom Stage Data (Prismatic) Listed below (Recalc) -Impervious
		:	

79,682 cf	Total A	Availa	ble	Storage
-----------	---------	--------	-----	---------

Elevation	Surt.Area	Inc.Store	Cum.Store	Wet.Area
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)	(sq-ft)
46.00	277	0	0	277
47.00	5,101	2,189	2,189	5,104
Elevation	Surf.Area	Inc.Store	Cum.Store	
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)	
47.00	5,101	0	0	
48.00	22,964	14,033	14,033	
49.00	27,625	25,295	39,327	
50.00	48,707	38,166	77,493	

Device	Routina	Invert	Outlet Devices
DEVICE	HUUUIIIU	IIIVEIL	Outlet Devices

#1 Discarded 46.00' **27.000 in/hr Exfiltration over Wetted area** 

**Discarded OutFlow** Max=3.19 cfs @ 11.97 hrs HW=47.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 3.19 cfs)

## Summary for Pond PP2: Stormtech SC-740 UGC

#### Top of Pond 47.6

Inflow Area = 8.813 ac, 83.39% Impervious, Inflow Depth = 6.80" for 100-yr 24 hr event Inflow = 44.05 cfs @ 12.26 hrs, Volume= 4.991 af Outflow = 24.25 cfs @ 12.56 hrs, Volume= 4.991 af, Atten= 45%, Lag= 17.6 min Discarded = 11.63 cfs @ 12.56 hrs, Volume= 4.193 af Primary = 12.61 cfs @ 12.56 hrs, Volume= 0.798 af

Routed to Link DP1\*: DP1\* (Proposed Condition)

#### 2482.H - HydroCAD

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Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.03 hrs Peak Elev= 47.44' @ 12.56 hrs Surf.Area= 16,865 sf Storage= 35,782 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 9.7 min (792.7 - 782.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	44.10'	14,790 cf	115.50'W x 146.02'L x 3.50'H Field A
			59,027 cf Overall - 22,051 cf Embedded = 36,976 cf x 40.0% Voids
#2A	44.60'	22,051 cf	ADS_StormTech SC-740 +Cap x 480 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			480 Chambers in 24 Rows
		36 842 cf	Total Available Storage

36,842 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	44.10'	27.000 in/hr Exfiltration over Wetted area
#2	Primary	44.61'	24.0" Round Culvert
			L= 29.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 44.61' / 44.32' S= 0.0100 '/' Cc= 0.900
			n= 0.012 Corrugated PP, smooth interior, Flow Area= 3.14 sf
#3	Device 2	44.61'	<b>34.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads
#4	Device 2	45.55'	<b>21.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads
#5	Device 2	46.40'	<b>12.0" W x 4.0" H Vert. Orifice/Grate</b> C= 0.600
			Limited to weir flow at low heads

**Discarded OutFlow** Max=11.63 cfs @ 12.56 hrs HW=47.44' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 11.63 cfs)

Primary OutFlow Max=12.60 cfs @ 12.56 hrs HW=47.44' (Free Discharge)

**-2=Culvert** (Passes 12.60 cfs of 19.84 cfs potential flow)

-3=Orifice/Grate (Orifice Controls 7.42 cfs @ 7.86 fps)

-4=Orifice/Grate (Orifice Controls 3.68 cfs @ 6.32 fps)

-5=Orifice/Grate (Orifice Controls 1.50 cfs @ 4.49 fps)

# APPENDIX C NRCS Soil Map & Data

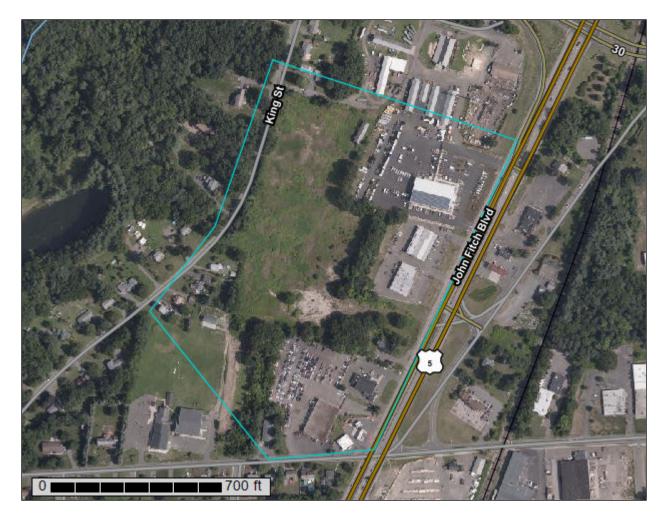


Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for State of Connecticut



# **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

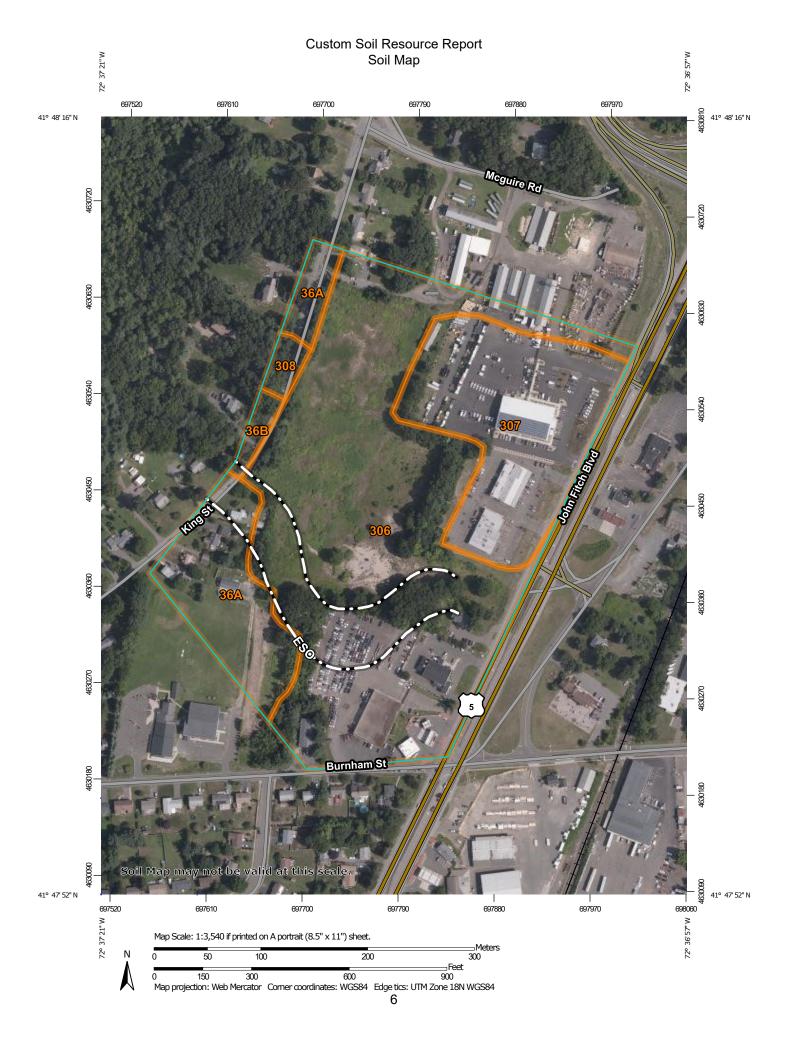
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# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons

Soil Map Unit Lines

Soil Map Unit Points

#### **Special Point Features**

Blowout (o)

Borrow Pit

Clay Spot

**Closed Depression** 

Gravel Pit

**Gravelly Spot** 

Landfill

Lava Flow Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

å

Spoil Area Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

#### **Water Features**

Streams and Canals

#### Transportation

---

Rails

Interstate Highways

**US Routes** 

00

Major Roads Local Roads

## Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut Survey Area Data: Version 21, Sep 7, 2021

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jul 15, 2019—Aug 29. 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
36A	Windsor loamy sand, 0 to 3 percent slopes	4.5	13.7%
Windsor loamy sand, 3 to 8 percent slopes		0.4	1.2%
306	Udorthents-Urban land complex	20.1	61.3%
307	Urban land	7.4	22.6%
308	Udorthents, smoothed	0.4	1.2%
Totals for Area of Interest	,	32.8	100.0%

# **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate

pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

#### **State of Connecticut**

#### 36A—Windsor loamy sand, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2svkg

Elevation: 0 to 990 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Windsor, loamy sand, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Windsor, Loamy Sand**

#### Setting

Landform: Outwash plains, outwash terraces, deltas, dunes

Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Parent material: Loose sandy glaciofluvial deposits derived from granite and/or loose sandy glaciofluvial deposits derived from schist and/or loose sandy

glaciofluvial deposits derived from gneiss

#### Typical profile

O - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loamy sand Bw - 3 to 25 inches: loamy sand C - 25 to 65 inches: sand

#### **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Deerfield, loamy sand

Percent of map unit: 10 percent

Landform: Deltas, terraces, outwash plains
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### Hinckley, loamy sand

Percent of map unit: 5 percent

Landform: Deltas, kames, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

rise

Down-slope shape: Convex

Across-slope shape: Convex, linear

Hydric soil rating: No

#### 36B—Windsor loamy sand, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2svkf

Elevation: 0 to 1,210 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Windsor, loamy sand, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Windsor, Loamy Sand**

#### Setting

Landform: Dunes, outwash plains, deltas, outwash terraces

Landform position (three-dimensional): Tread, riser

Down-slope shape: Convex, linear Across-slope shape: Convex, linear

Parent material: Loose sandy glaciofluvial deposits derived from granite and/or loose sandy glaciofluvial deposits derived from schist and/or loose sandy glaciofluvial deposits derived from gneiss

\_\_\_\_\_

#### **Typical profile**

O - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loamy sand

Bw - 3 to 25 inches: loamy sand C - 25 to 65 inches: sand

#### **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.5 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Hinckley, loamy sand

Percent of map unit: 10 percent

Landform: Deltas, kames, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

rise

Down-slope shape: Convex

Across-slope shape: Convex, linear

Hydric soil rating: No

#### Deerfield, loamy sand

Percent of map unit: 5 percent

Landform: Deltas, terraces, outwash plains
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

#### 306—Udorthents-Urban land complex

#### Map Unit Setting

National map unit symbol: 9lmg

Elevation: 0 to 2,000 feet

Mean annual precipitation: 43 to 56 inches
Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 120 to 185 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Udorthents and similar soils: 50 percent

Urban land: 35 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Udorthents**

#### Setting

Down-slope shape: Convex Across-slope shape: Linear Parent material: Drift

#### **Typical profile**

A - 0 to 5 inches: loam

C1 - 5 to 21 inches: gravelly loam

C2 - 21 to 80 inches: very gravelly sandy loam

#### **Properties and qualities**

Slope: 0 to 25 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00

to 1.98 in/hr)

Depth to water table: About 54 to 72 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: B Hydric soil rating: No

#### **Description of Urban Land**

#### Typical profile

H - 0 to 6 inches: material

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: Unranked

#### **Minor Components**

#### Unnamed, undisturbed soils

Percent of map unit: 8 percent

Hydric soil rating: No

#### **Udorthents, wet substratum**

Percent of map unit: 5 percent

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### **Rock outcrop**

Percent of map unit: 2 percent

Hydric soil rating: No

#### 307—Urban land

#### **Map Unit Setting**

National map unit symbol: 9lmh Elevation: 0 to 2,000 feet

Mean annual precipitation: 43 to 56 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 120 to 185 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Urban land: 80 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Urban Land**

#### **Typical profile**

H - 0 to 6 inches: material

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: Unranked

#### **Minor Components**

#### Udorthents, wet substratum

Percent of map unit: 10 percent Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Unnamed, undisturbed soils

Percent of map unit: 10 percent

Hydric soil rating: No

#### 308—Udorthents, smoothed

#### **Map Unit Setting**

National map unit symbol: 9lmj Elevation: 0 to 2,000 feet

Mean annual precipitation: 43 to 56 inches Mean annual air temperature: 45 to 55 degrees F

Frost-free period: 120 to 185 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Udorthents and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Udorthents**

#### Setting

Down-slope shape: Convex Across-slope shape: Linear

#### **Typical profile**

A - 0 to 5 inches: loam

C1 - 5 to 21 inches: gravelly loam

C2 - 21 to 80 inches: very gravelly sandy loam

#### **Properties and qualities**

Slope: 0 to 35 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to high (0.00

to 1.98 in/hr)

Depth to water table: About 24 to 54 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 6.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: C Hydric soil rating: No

#### **Minor Components**

#### Udorthents, wet substratum

Percent of map unit: 7 percent

Hydric soil rating: No

#### Unnamed, undisturbed soils

Percent of map unit: 7 percent Hydric soil rating: No

#### **Urban land**

Percent of map unit: 5 percent Hydric soil rating: No

#### Rock outcrop

Percent of map unit: 1 percent Hydric soil rating: No

# Soil Information for All Uses

# **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

#### Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

# **Hydrologic Soil Group**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

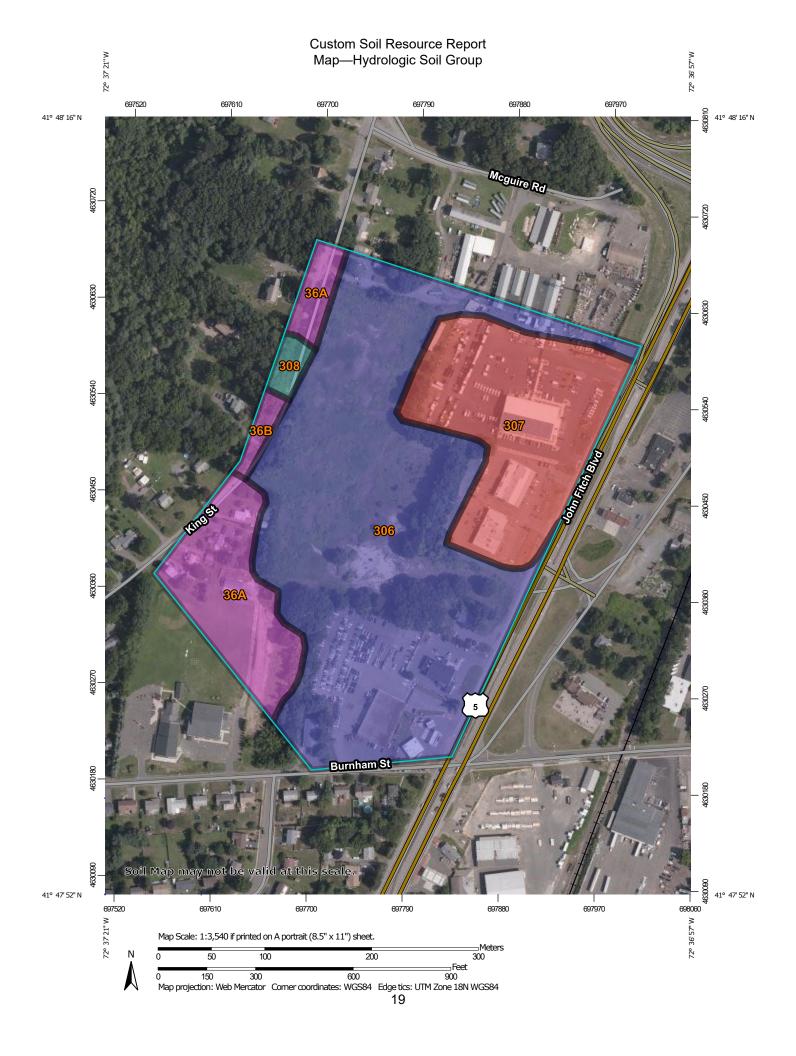
Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



#### MAP LEGEND MAP INFORMATION Area of Interest (AOI) The soil surveys that comprise your AOI were mapped at С 1:12.000. Area of Interest (AOI) C/D Soils D Warning: Soil Map may not be valid at this scale. Soil Rating Polygons Not rated or not available Α Enlargement of maps beyond the scale of mapping can cause **Water Features** A/D misunderstanding of the detail of mapping and accuracy of soil Streams and Canals line placement. The maps do not show the small areas of В contrasting soils that could have been shown at a more detailed Transportation scale. B/D Rails ---Interstate Highways Please rely on the bar scale on each map sheet for map C/D **US Routes** measurements. Major Roads Source of Map: Natural Resources Conservation Service Not rated or not available Local Roads Web Soil Survey URL: -Coordinate System: Web Mercator (EPSG:3857) Soil Rating Lines Background Aerial Photography Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: State of Connecticut Not rated or not available Survey Area Data: Version 21, Sep 7, 2021 **Soil Rating Points** Soil map units are labeled (as space allows) for map scales Α 1:50.000 or larger. A/D Date(s) aerial images were photographed: Jul 15, 2019—Aug 29. 2019 B/D The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

### Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
36A	Windsor loamy sand, 0 to 3 percent slopes	А	4.5	13.7%
36B	Windsor loamy sand, 3 to 8 percent slopes	А	0.4	1.2%
306	Udorthents-Urban land complex	В	20.1	61.3%
307	Urban land	D	7.4	22.6%
308	Udorthents, smoothed	С	0.4	1.2%
Totals for Area of Intere	est	32.8	100.0%	

## Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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## APPENDIX D NOAA Rainfall Data



NOAA Atlas 14, Volume 10, Version 3 Location name: South Windsor, Connecticut, USA\* Latitude: 41.8019°, Longitude: -72.6202° Elevation: 54.7 ft\*\* source: ESRI Maps
\*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite NOAA, National Weather Service, Silver Spring, Maryland

#### PF tabular | PF graphical | Maps & aerials

#### PF tabular

Duration				Avera	ge recurren	ce interval (y	years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	<b>4.01</b> (3.14-5.11)	<b>4.87</b> (3.82-6.22)	<b>6.28</b> (4.90-8.03)	<b>7.44</b> (5.77-9.58)	<b>9.04</b> (6.78-12.2)	<b>10.2</b> (7.54-14.1)	<b>11.5</b> (8.21-16.5)	<b>12.9</b> (8.72-19.0)	<b>15.0</b> (9.71-22.8)	<b>16.6</b> (10.5-25.9)
10-min	<b>2.84</b> (2.23-3.62)	<b>3.45</b> (2.70-4.40)	<b>4.44</b> (3.47-5.69)	<b>5.27</b> (4.09-6.78)	<b>6.40</b> (4.80-8.63)	<b>7.25</b> (5.33-10.0)	<b>8.15</b> (5.81-11.7)	<b>9.16</b> (6.17-13.5)	<b>10.6</b> (6.87-16.2)	<b>11.8</b> (7.46-18.3)
15-min	<b>2.23</b> (1.75-2.84)	<b>2.71</b> (2.12-3.45)	<b>3.49</b> (2.72-4.46)	<b>4.13</b> (3.20-5.32)	<b>5.02</b> (3.76-6.77)	<b>5.69</b> (4.18-7.85)	<b>6.39</b> (4.56-9.17)	<b>7.18</b> (4.84-10.6)	<b>8.31</b> (5.39-12.7)	<b>9.24</b> (5.85-14.4)
30-min	<b>1.49</b> (1.17-1.90)	<b>1.82</b> (1.42-2.32)	<b>2.34</b> (1.83-3.00)	<b>2.78</b> (2.16-3.58)	<b>3.39</b> (2.54-4.57)	<b>3.85</b> (2.82-5.31)	<b>4.32</b> (3.08-6.20)	<b>4.86</b> (3.28-7.14)	<b>5.62</b> (3.65-8.57)	<b>6.25</b> (3.96-9.73)
60-min	<b>0.936</b> (0.733-1.19)	<b>1.14</b> (0.893-1.45)	<b>1.48</b> (1.15-1.89)	<b>1.75</b> (1.36-2.26)	<b>2.13</b> (1.60-2.88)	<b>2.42</b> (1.78-3.34)	<b>2.72</b> (1.94-3.91)	<b>3.06</b> (2.07-4.50)	<b>3.55</b> (2.30-5.40)	<b>3.94</b> (2.49-6.14)
2-hr	<b>0.608</b> (0.479-0.769)	<b>0.736</b> (0.580-0.932)	<b>0.946</b> (0.742-1.20)	<b>1.12</b> (0.874-1.43)	<b>1.36</b> (1.03-1.83)	<b>1.54</b> (1.14-2.12)	<b>1.73</b> (1.25-2.48)	<b>1.96</b> (1.32-2.86)	<b>2.29</b> (1.49-3.47)	<b>2.57</b> (1.63-3.98)
3-hr	<b>0.466</b> (0.369-0.588)	<b>0.564</b> (0.446-0.713)	<b>0.725</b> (0.570-0.919)	<b>0.858</b> (0.671-1.09)	<b>1.04</b> (0.790-1.40)	<b>1.18</b> (0.875-1.62)	<b>1.32</b> (0.958-1.90)	<b>1.50</b> (1.02-2.18)	<b>1.77</b> (1.15-2.67)	<b>1.99</b> (1.27-3.07)
6-hr	<b>0.292</b> (0.232-0.366)	<b>0.355</b> (0.282-0.445)	<b>0.457</b> (0.362-0.576)	<b>0.542</b> (0.427-0.687)	<b>0.659</b> (0.503-0.879)	<b>0.745</b> (0.558-1.02)	<b>0.839</b> (0.612-1.20)	<b>0.954</b> (0.649-1.38)	<b>1.13</b> (0.739-1.70)	<b>1.29</b> (0.820-1.97)
12-hr	<b>0.176</b> (0.141-0.220)	<b>0.216</b> (0.173-0.269)	<b>0.281</b> (0.224-0.352)	<b>0.335</b> (0.265-0.422)	<b>0.409</b> (0.314-0.543)	<b>0.464</b> (0.349-0.632)	<b>0.523</b> (0.384-0.746)	<b>0.598</b> (0.408-0.859)	<b>0.713</b> (0.467-1.06)	<b>0.812</b> (0.520-1.24)
24-hr	<b>0.103</b> (0.083-0.128)	<b>0.128</b> (0.103-0.159)	<b>0.169</b> (0.136-0.211)	<b>0.203</b> (0.162-0.255)	<b>0.250</b> (0.194-0.331)	<b>0.285</b> (0.216-0.387)	<b>0.323</b> (0.239-0.460)	<b>0.371</b> (0.254-0.531)	<b>0.448</b> (0.295-0.664)	<b>0.516</b> (0.331-0.779
2-day	<b>0.058</b> (0.047-0.072)	<b>0.074</b> (0.060-0.091)	<b>0.099</b> (0.080-0.122)	<b>0.120</b> (0.096-0.149)	<b>0.148</b> (0.116-0.196)	<b>0.169</b> (0.129-0.230)	<b>0.192</b> (0.144-0.275)	<b>0.224</b> (0.154-0.318)	<b>0.275</b> (0.181-0.405)	<b>0.321</b> (0.206-0.481
3-day	<b>0.042</b> (0.034-0.052)	<b>0.054</b> (0.044-0.066)	<b>0.072</b> (0.058-0.089)	<b>0.087</b> (0.070-0.108)	<b>0.108</b> (0.085-0.143)	<b>0.123</b> (0.095-0.167)	<b>0.141</b> (0.106-0.201)	<b>0.164</b> (0.113-0.232)	<b>0.202</b> (0.133-0.297)	<b>0.237</b> (0.153-0.354
4-day	<b>0.034</b> (0.028-0.042)	<b>0.043</b> (0.035-0.053)	<b>0.058</b> (0.047-0.071)	<b>0.070</b> (0.056-0.086)	<b>0.087</b> (0.068-0.114)	<b>0.099</b> (0.076-0.133)	<b>0.112</b> (0.085-0.160)	<b>0.131</b> (0.090-0.185)	<b>0.162</b> (0.107-0.236)	<b>0.189</b> (0.122-0.282
7-day	<b>0.023</b> (0.019-0.028)	<b>0.029</b> (0.023-0.035)	<b>0.038</b> (0.031-0.046)	<b>0.046</b> (0.037-0.056)	<b>0.056</b> (0.044-0.074)	<b>0.064</b> (0.050-0.086)	<b>0.073</b> (0.055-0.103)	<b>0.085</b> (0.059-0.119)	<b>0.104</b> (0.069-0.151)	<b>0.121</b> (0.078-0.179
10-day	<b>0.019</b> (0.015-0.022)	<b>0.023</b> (0.019-0.028)	<b>0.030</b> (0.024-0.036)	<b>0.035</b> (0.029-0.043)	<b>0.043</b> (0.034-0.056)	<b>0.049</b> (0.038-0.065)	<b>0.056</b> (0.042-0.078)	<b>0.064</b> (0.044-0.089)	<b>0.077</b> (0.051-0.112)	<b>0.089</b> (0.058-0.132
20-day	<b>0.013</b> (0.011-0.016)	<b>0.016</b> (0.013-0.019)	<b>0.019</b> (0.016-0.023)	<b>0.022</b> (0.018-0.027)	<b>0.026</b> (0.021-0.034)	<b>0.030</b> (0.023-0.039)	<b>0.033</b> (0.025-0.045)	<b>0.037</b> (0.026-0.051)	<b>0.043</b> (0.029-0.062)	<b>0.048</b> (0.032-0.071
30-day	<b>0.011</b> (0.009-0.013)	<b>0.013</b> (0.011-0.015)	<b>0.015</b> (0.013-0.018)	<b>0.017</b> (0.014-0.021)	<b>0.020</b> (0.016-0.026)	<b>0.022</b> (0.017-0.029)	<b>0.025</b> (0.018-0.033)	<b>0.027</b> (0.019-0.037)	<b>0.031</b> (0.021-0.044)	<b>0.034</b> (0.022-0.049
45-day	<b>0.009</b> (0.008-0.011)	<b>0.011</b> (0.009-0.013)	<b>0.012</b> (0.010-0.015)	<b>0.014</b> (0.011-0.017)	<b>0.016</b> (0.012-0.020)	<b>0.017</b> (0.013-0.022)	<b>0.019</b> (0.014-0.025)	<b>0.020</b> (0.014-0.028)	<b>0.022</b> (0.015-0.032)	<b>0.024</b> (0.016-0.035
60-day	0.008	0.009	0.010	0.012 (0.010-0.014)	0.013	0.014	0.015	0.017	0.018	0.019

<sup>&</sup>lt;sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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#### PF graphical



NOAA Atlas 14, Volume 10, Version 3
Location name: South Windsor, Connecticut, USA\*
Latitude: 41.8019°, Longitude: -72.6202°
Elevation: 54.7 ft\*\*

\* source: ESRI Maps
\*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>												
Duration				Average i	recurrence	interval (y	ears)					
Duration	1	2	5	10	25	50	100	200	500	1000		
5-min	<b>0.334</b> (0.262-0.426)	<b>0.334 0.406 0.523</b> (0.318-0.518) (0.408-0.669		<b>0.620</b> (0.481-0.798)	<b>0.753</b> (0.565-1.02)	<b>0.854</b> (0.628-1.18)	<b>0.959</b> (0.684-1.38)	<b>1.08</b> (0.727-1.58)	<b>1.25</b> (0.809-1.90)	<b>1.39</b> (0.877-2.16)		
10-min	<b>0.474</b> (0.371-0.604)	<b>0.575</b> (0.450-0.733)	<b>0.740</b> (0.578-0.949)	<b>0.878</b> (0.681-1.13)	<b>1.07</b> (0.800-1.44)	<b>1.21</b> (0.889-1.67)	<b>1.36</b> (0.968-1.95)	<b>1.53</b> (1.03-2.24)	<b>1.77</b> (1.15-2.69)	<b>1.96</b> (1.24-3.06)		
15-min	<b>0.557</b> (0.437-0.710)	<b>0.677</b> (0.530-0.863)	<b>0.872</b> (0.681-1.12)			<b>1.42</b> (1.05-1.96)	<b>1.60</b> (1.14-2.29)	<b>1.80</b> (1.21-2.64)	<b>2.08</b> (1.35-3.17)	<b>2.31</b> (1.46-3.60)		
30-min	<b>0.747</b> (0.585-0.951)	<b>0.908</b> (0.711-1.16)	<b>1.17</b> (0.915-1.50)	<b>1.39</b> (1.08-1.79)	<b>1.70</b> (1.27-2.29)	<b>1.92</b> (1.41-2.65)	<b>2.16</b> (1.54-3.10)	<b>2.43</b> (1.64-3.57)	<b>2.81</b> (1.82-4.29)	<b>3.13</b> (1.98-4.87)		
60-min	<b>0.936</b> (0.733-1.19)	<b>1.14</b> (0.893-1.45)	<b>1.48</b> (1.15-1.89)	<b>1.75</b> (1.36-2.26)	<b>2.13</b> (1.60-2.88)	<b>2.42</b> (1.78-3.34)	<b>2.72</b> (1.94-3.91)	<b>3.06</b> (2.07-4.50)	<b>3.55</b> (2.30-5.40)	<b>3.94</b> (2.49-6.14)		
2-hr	<b>1.22</b> (0.958-1.54)	<b>1.47</b> (1.16-1.87)	<b>1.89</b> (1.49-2.41)	<b>2.24</b> (1.75-2.87)	<b>2.72</b> (2.06-3.66)	<b>3.08</b> (2.28-4.24)	<b>3.46</b> (2.49-4.97)	<b>3.91</b> (2.65-5.71)	<b>4.58</b> (2.98-6.94)	<b>5.14</b> (3.26-7.96)		
3-hr	<b>1.40</b> (1.11-1.77)	<b>1.70</b> (1.34-2.14)	<b>2.18</b> (1.71-2.76)	<b>2.58</b> (2.02-3.29)	<b>3.13</b> (2.37-4.19)	<b>3.53</b> (2.63-4.86)	<b>3.97</b> (2.88-5.70)	<b>4.50</b> (3.05-6.55)	<b>5.30</b> (3.45-8.01)	<b>5.99</b> (3.81-9.22)		
6-hr	<b>1.75</b> (1.39-2.19)	<b>2.12</b> (1.69-2.67)	<b>2.74</b> (2.17-3.45)	<b>3.25</b> (2.56-4.11)	<b>3.94</b> (3.01-5.27)	<b>4.46</b> (3.34-6.11)	<b>5.02</b> (3.66-7.19)	<b>5.71</b> (3.89-8.27)	<b>6.78</b> (4.43-10.2)	<b>7.69</b> (4.91-11.8)		
12-hr	<b>2.12</b> (1.70-2.65)	<b>2.60</b> (2.08-3.25)	<b>3.39</b> (2.70-4.24)	<b>4.04</b> (3.20-5.08)	<b>4.93</b> (3.79-6.55)	<b>5.59</b> (4.21-7.61)	<b>6.31</b> (4.63-8.99)	<b>7.20</b> (4.92-10.4)	<b>8.59</b> (5.63-12.8)	<b>9.79</b> (6.26-14.9)		
24-hr	<b>2.47</b> (1.99-3.06)	<b>3.08</b> (2.48-3.81)	<b>4.06</b> (3.26-5.06)	<b>4.88</b> (3.89-6.11)	<b>6.01</b> (4.65-7.95)	<b>6.83</b> (5.19-9.29)	<b>7.75</b> (5.74-11.0)	<b>8.91</b> (6.10-12.7)	<b>10.8</b> (7.07-15.9)	<b>12.4</b> (7.95-18.7)		
2-day	<b>2.80</b> (2.27-3.44)	<b>3.53</b> (2.86-4.35)	<b>4.74</b> (3.82-5.86)	<b>5.74</b> (4.60-7.14)	<b>7.12</b> (5.55-9.40)	<b>8.11</b> (6.21-11.0)	<b>9.24</b> (6.93-13.2)	<b>10.7</b> (7.37-15.3)	<b>13.2</b> (8.70-19.4)	<b>15.4</b> (9.91-23.1)		
3-day	<b>3.04</b> (2.48-3.73)	<b>3.86</b> (3.13-4.73)	<b>5.18</b> (4.19-6.38)	<b>6.28</b> (5.05-7.78)	<b>7.79</b> (6.10-10.3)	<b>8.89</b> (6.83-12.0)	<b>10.1</b> (7.63-14.5)	<b>11.8</b> (8.12-16.7)	<b>14.6</b> (9.61-21.4)	<b>17.0</b> (11.0-25.5)		
4-day	<b>3.26</b> (2.66-3.99)	<b>4.12</b> (3.36-5.05)	<b>5.53</b> (4.49-6.80)	<b>6.70</b> (5.40-8.28)	<b>8.31</b> (6.52-10.9)	<b>9.47</b> (7.30-12.8)	<b>10.8</b> (8.15-15.4)	<b>12.6</b> (8.66-17.8)	<b>15.5</b> (10.3-22.7)	<b>18.2</b> (11.7-27.1)		
7-day	<b>3.85</b> (3.16-4.68)	<b>4.81</b> (3.94-5.86)	<b>6.39</b> (5.21-7.81)	<b>7.69</b> (6.23-9.46)	<b>9.49</b> (7.47-12.4)	<b>10.8</b> (8.34-14.5)	<b>12.3</b> (9.26-17.3)	<b>14.2</b> (9.83-20.0)	<b>17.4</b> (11.5-25.3)	<b>20.3</b> (13.1-30.0)		
10-day	<b>4.45</b> (3.66-5.40)	<b>5.47</b> (4.49-6.64)	<b>7.13</b> (5.83-8.68)	<b>8.50</b> (6.91-10.4)	<b>10.4</b> (8.20-13.5)	<b>11.8</b> (9.11-15.7)	<b>13.3</b> (10.0-18.6)	<b>15.3</b> (10.6-21.4)	<b>18.6</b> (12.3-26.9)	<b>21.4</b> (13.9-31.7)		
20-day	<b>6.41</b> (5.30-7.72)	<b>7.48</b> (6.18-9.02)	<b>9.23</b> (7.60-11.2)	<b>10.7</b> (8.74-13.0)	<b>12.7</b> (10.0-16.2)	<b>14.2</b> (10.9-18.6)	<b>15.8</b> (11.8-21.6)	<b>17.7</b> (12.4-24.6)	<b>20.7</b> (13.8-29.8)	<b>23.3</b> (15.1-34.1)		
30-day	<b>8.09</b> (6.72-9.72)	<b>9.19</b> (7.62-11.0)	<b>11.0</b> (9.08-13.3)	<b>12.5</b> (10.2-15.1)	<b>14.5</b> (11.5-18.4)	<b>16.1</b> (12.4-20.8)	<b>17.7</b> (13.2-23.8)	<b>19.5</b> (13.7-26.9)	<b>22.2</b> (14.9-31.7)	<b>24.4</b> (15.9-35.7)		
45-day	<b>10.2</b> (8.52-12.2)	<b>11.4</b> (9.45-13.6)	<b>13.2</b> (11.0-15.9)	<b>14.8</b> (12.2-17.8)	<b>16.9</b> (13.4-21.2)	<b>18.5</b> (14.3-23.7)	<b>20.1</b> (14.9-26.7)	<b>21.8</b> (15.4-30.0)	<b>24.1</b> (16.2-34.3)	<b>25.9</b> (16.9-37.7)		
60-day	<b>12.0</b> (10.0-14.3)	<b>13.2</b> (11.0-15.8)	<b>15.1</b> (12.6-18.1)	<b>16.7</b> (13.8-20.1)	<b>18.9</b> (15.0-23.6)	<b>20.6</b> (15.9-26.3)	<b>22.3</b> (16.5-29.3)	<b>23.9</b> (16.9-32.7)	<b>25.9</b> (17.5-36.7)	<b>27.3</b> (17.9-39.7)		

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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#### PF graphical

## APPENDIX E Storm Sewer Analysis

## **Storm Sewer Tabulation**

Stati	on	Len	Drng A	\rea	Rnoff	Area x	С	Тс		Rain	Total		Vel	Pipe		Invert Ele	ev	HGL Elev		Grnd / Rim Elev		Line ID
Line			Incr	Total	coeff	Incr	Total	Inlet	Syst	(1)	flow	full		Size	Slope	Dn	Up	Dn	Up	Dn	Up	
	Line	(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	20	0.70	6.73	0.90	0.63	5.01	6.0	22.0	3.4	16.96	18.17	6.66	24	0.55	44.87	44.98	46.35	46.52	47.38	50.00	CB4-DMH2
2	1	130	0.61	0.61	0.90	0.55	0.55	6.0	6.0	6.9	3.77	4.95	4.40	15	0.50	46.95	47.60	47.81	48.39	50.00	50.10	CB5-CB4
3	1	222	0.61	2.94	0.90	0.55	1.74	6.0	20.9	3.5	6.06	7.97	3.43	18	0.49	45.53	46.62	47.81	48.44	50.00	50.10	CB6-CB4
4	3	196	2.33	2.33	0.51	1.19	1.19	20.0	20.0	3.6	4.27	4.57	3.48	15	0.50	46.62	47.60	48.62	49.47	50.10	50.10	CB7-CB6
5	1	102	0.00	2.48	0.00	0.00	2.10	0.0	7.8	6.1	12.71	17.49	4.05	24	0.51	44.98	45.50	47.81	48.08	50.00	51.40	DMH5-CB4
6	5	130	0.44	0.44	0.73	0.32	0.32	7.0	7.0	6.4	2.06	2.77	2.62	12	0.52	46.33	47.00	48.31	48.68	51.40	49.50	CB9-DMH5
7	5	148	2.04	2.04	0.87	1.77	1.77	6.0	6.0	6.9	12.20	12.33	4.97	15(2b)	0.78	45.50	46.65	48.31	49.44	51.40	49.35	CB8-DMH5
8	End	9	0.26	0.26	0.90	0.23	0.23	6.0	6.0	6.9	1.61	29.95	3.50	15	18.33	45.35	47.00	45.85	47.50	-1.99	50.00	CB1-UGC
9	End	100	0.22	0.22	0.90	0.20	0.20	6.0	6.0	6.9	1.36	10.59	3.32	15	2.29	44.71	47.00	45.17	47.46	47.65	49.50	CB2-UGC
10	End	26	1.56	1.56	0.90	1.40	1.40	6.0	6.0	6.9	9.65	16.35	8.07	15	5.46	44.71	46.13	45.88	47.30	47.59	49.00	CB3-UGC
11	End	35	3.60	5.80	0.48	1.73	2.83	53.0	53.0	1.9	5.39	8.38	4.32	18	0.54	42.29	42.48	43.43	43.37	49.64	47.70	YD2-EXDMH
12	11	87	0.00	2.20	0.00	0.00	1.10	0.0	7.6	6.2	6.77	8.18	5.17	18	0.52	42.48	42.93	43.52	43.97	47.70	50.50	DMH1-YD2
13	12	170	2.20	2.20	0.50	1.10	1.10	7.0	7.0	6.4	7.04	8.14	4.78	18	0.51	42.93	43.80	44.26	44.85	50.50	46.50	YD1-DMH1

Project File: 2482.H - Storm Sewer.stm Number of lines: 13 Run Date: 6/13/2022

NOTES:Intensity = 35.85 / (Inlet time + 3.70) ^ 0.73; Return period =Yrs. 10; c = cir e = ellip b = box

# APPENDIX F Water Quality Flow Calculations and Data

#### 45, 95 John Fitch Boulevard and 542 King Street- DPI No. 2482.H

June 13, 2022

#### WQF To Underground Chamber System – Watershed P3

```
To find Unit Peak Discharge qu with Exhibit 4-III, the following is needed:
        Time of Concentration (Tc):
                 20 \text{ mins} = 0.33 \text{ hours}
        Initial Abstraction (Ia) in inches / Design Precipitation (P) in inches:
                Initial abstraction (Ia) from Table 4-I in Chapter 4 of TR-55 needs Curve Number (CN)
                         CN = 92
                Ia = 0.174 inches
                Design Precipitation (P) = 1" for water quality storms per Appendix B
        Ia/P = 0.174
Unit Peak Discharge qu = \frac{435}{\text{cfs/mi}^2/\text{inch}}
Drainage Area A = 383,881 \text{ sf} = 8.813 \text{ acres} = 0.0138 \text{ mi}^2
Runoff Depth Q = WQV (acre-feet) x 12 / drainage area (acres)
        Water Quality Volume (WQV) = (1")(R)(A)/12, where:
                R = volumetric runoff coefficient
                         = 0.05 + 0.009(I), where I = percent impervious cover = 83.39\%
                R = 0.05 + 0.009(I)
                R = 0.05 + 0.009(83.39)
                R = 0.801
                A = drainage area in acres = 0.547 acres
        WQV = (1")(R)(A)/12
        WQV = (1")(0.801)(8.813 \text{ acres}) / 12 \text{ in/ft}
        WQV = 0.5883 acre-feet
O = (WOV X 12 in/ft)/Drainage Area
Q = (0.5883 \text{ acre-feet x } 12 \text{ in/ft}) / 8.813 \text{ acres}
Q = 0.801 \text{ in}
WOF = qu \times A \times O
WQF = 435 \text{ cfs/mi}^2/\text{inch } \times 0.0138 \text{ mi}^2 \times 0.801 \text{ in}
WQF = 4.81 cfs required
```

#### **Proposed BMP**

As shown on the enclosed water quality per unit sizing report, the proposed ADS Stormtech row (utilizing at least 34 ~ SC-740 chambers @ 0.15 cfs treated flow rate per chamber) is rated for 80% TSS removal efficiency for the required 4.81 cfs water quality flow. The current design plan proposes 40 isolator row chambers for the subject area, providing 6.0 cfs of WQF. See isolator row sizing chart included in the appendix.



Division of

STORMTECH ISOLATOR ROW SIZING CHART												
SC-160LP SC-310 SC-740 DC-780 MC-3500 MC-45												
Chamber Area (Sq.Ft.)	11.4	20	27.8	27.8	43.2	30.1						
Treated Flow Rate per chamber (CFS)	0.055	0.11	0.15	0.15	0.24	0.17						

**NOTE:** Testing of the Isolator Row verified by NJCAT.It has shown to have a TSS removal efficiency of 84% for SIL-CO-SIL 250. MASTEP verification of up to 83% TSS of the OK-110.

NJCAT verified Treated Flow Rate (GPM / Sq.Ft.) 2



For more information contact ADS at 800-821-6710 or visit www.ads-pipe.com



## APPENDIX G Drainage Area Maps

e: GN jobs N 2482 N 2482 N Engineering N Stormwater N 2482 - Drainage Map.dwg Layout, O2 C-DA2 Plotted; 6/13/2022 124 PM Last Saved; 6/13/2022 1:14 PM Last Saved By: Matthew. Viens